



**Dr. Stephan
ARNDT**

Head of Technology &
Innovation
Mining One

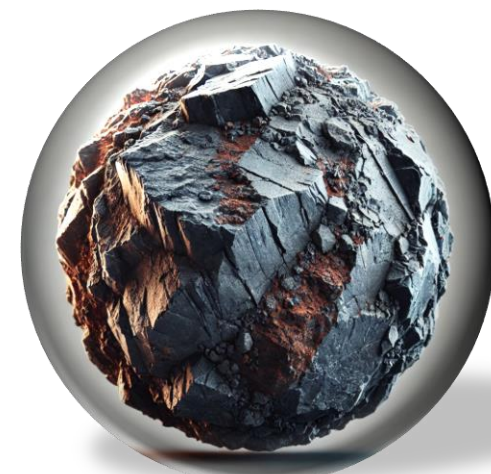
A decorative graphic on the left side of the slide, featuring a network of interconnected nodes in various colors (red, yellow, orange, black, white, blue) with thin lines connecting them, set against a glowing blue background.

EXTREME ENVIRONMENTS: HOW HPC
SIMULATION HELPS EXTRACTING VALUABLE
RESOURCES

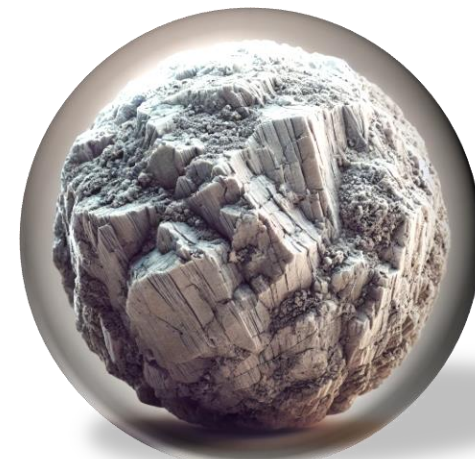
Extracting Resources

The mining industry has an image problem – Sustainability – A global skills crisis – Decarbonisation, Electric Vehicles and Green Steel – Digital Twins

The World Needs Resources



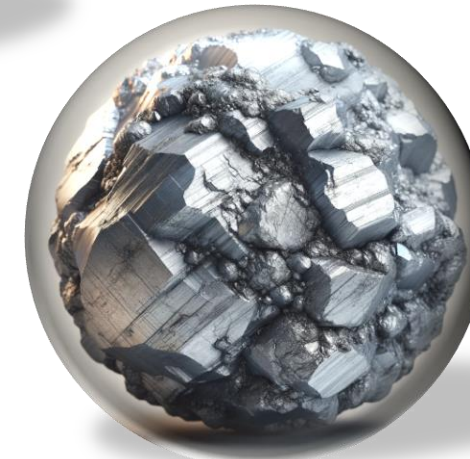
Iron Ore



Lithium



Nickel



Zinc



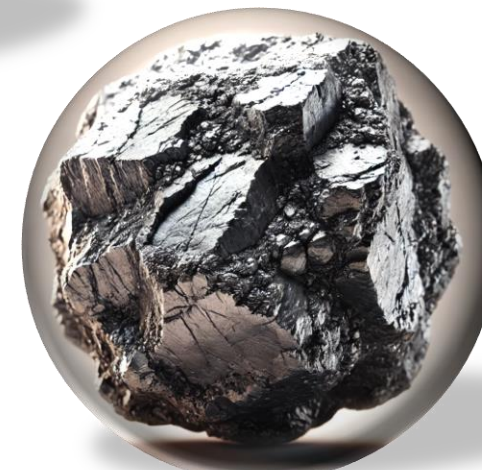
Rare Earth



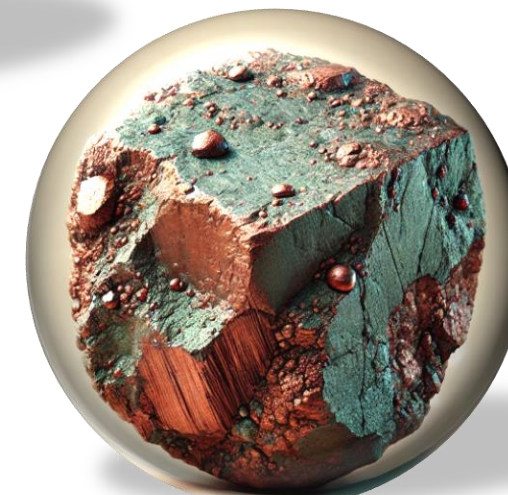
Cobalt



Gold



Silver



Copper



Aluminium

Extreme Environments

4000m Altitude – or 1200m below the surface – Scale

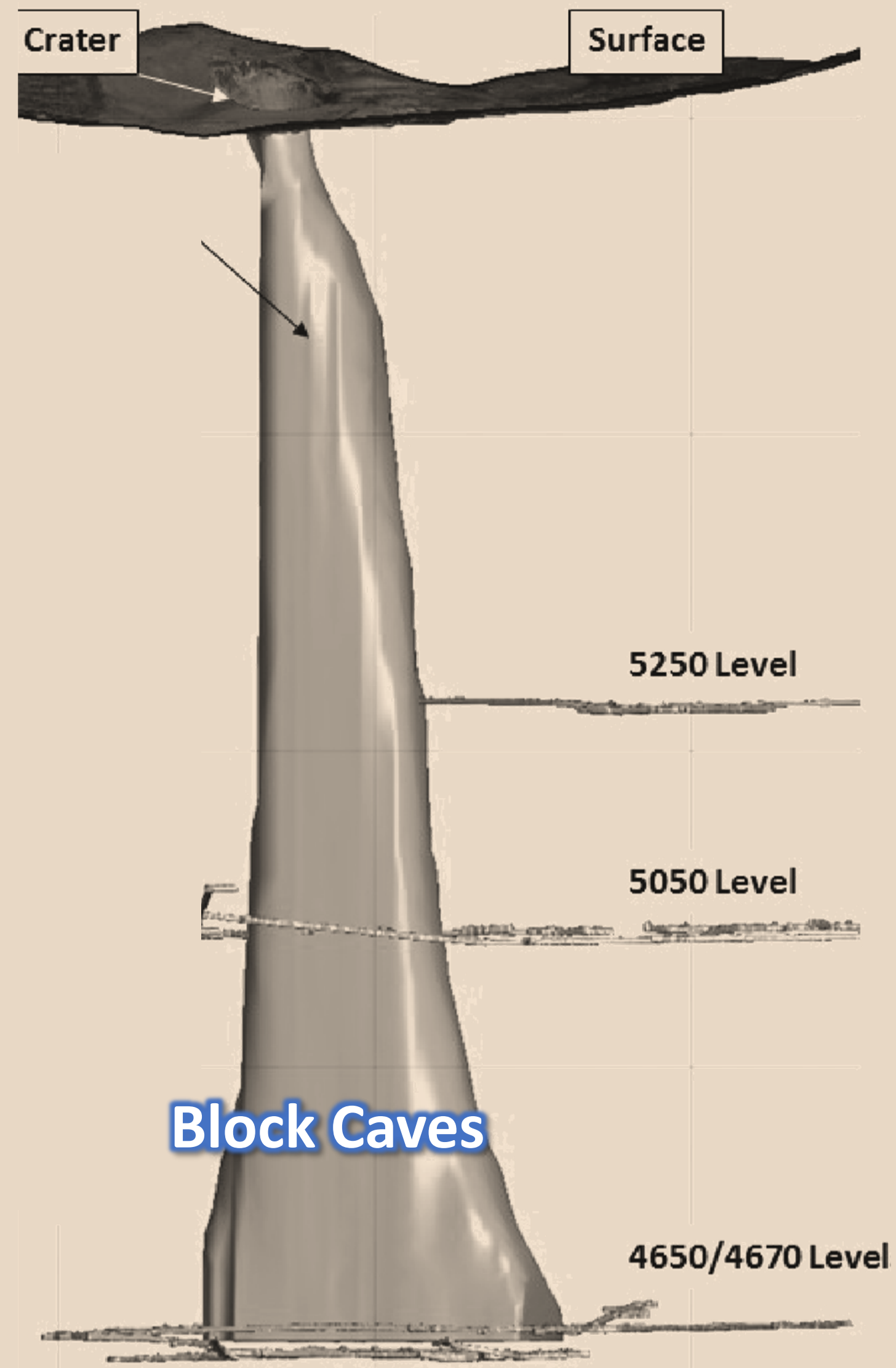
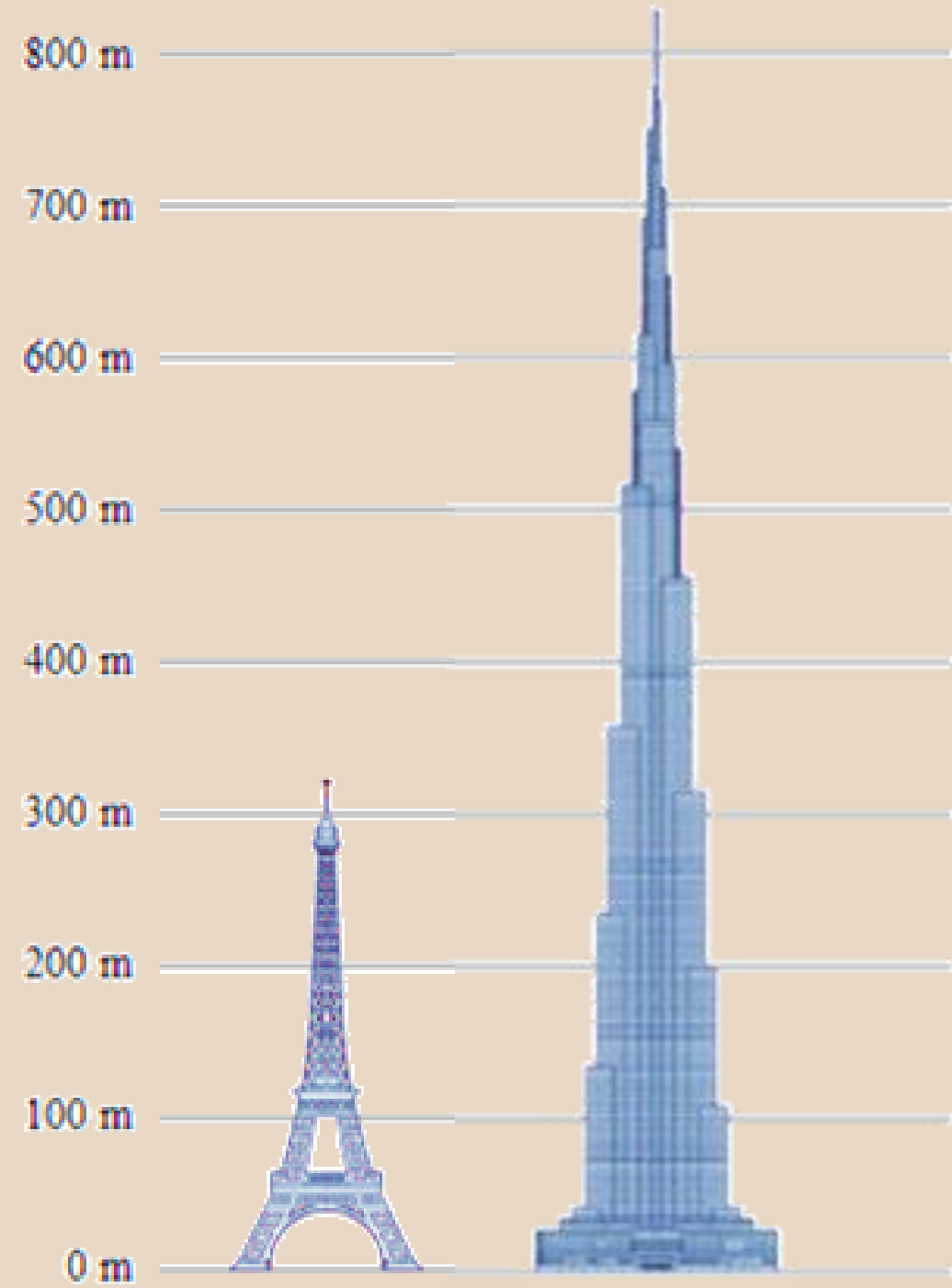
Extreme Environments – 4000m Altitude



The World's highest altitude Abaqus Training?



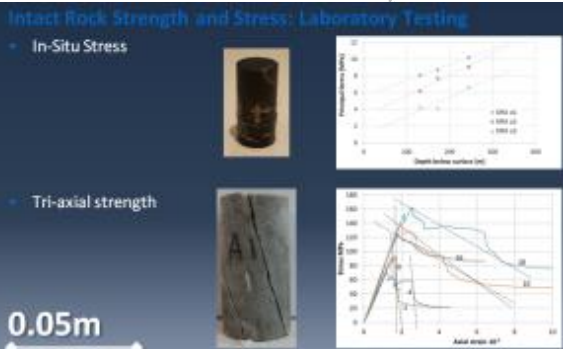
1200m Deep ... and Beyond



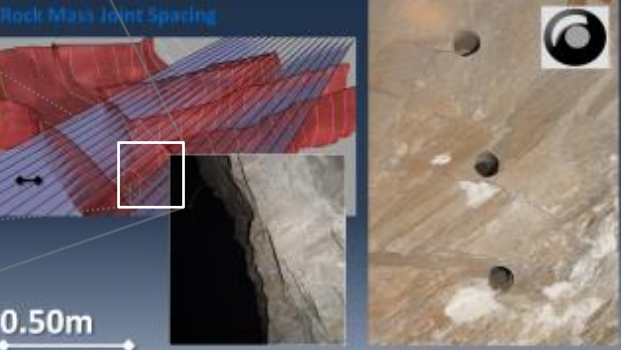
Extreme Environments – Scale

Forecasting Seismicity, Stability and Stress in Underground Mining
Stephan Arndt, 2013 SIMULIA Community Conference, Vienna

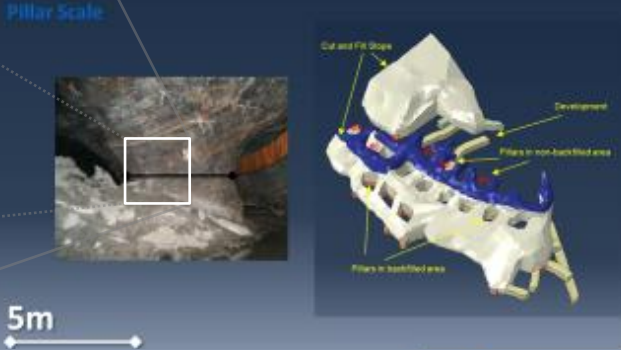
0.05m



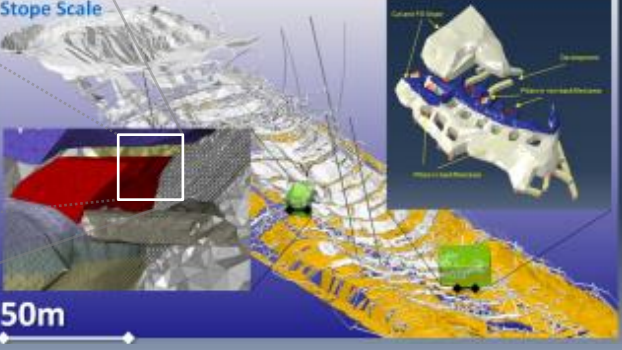
0.5m



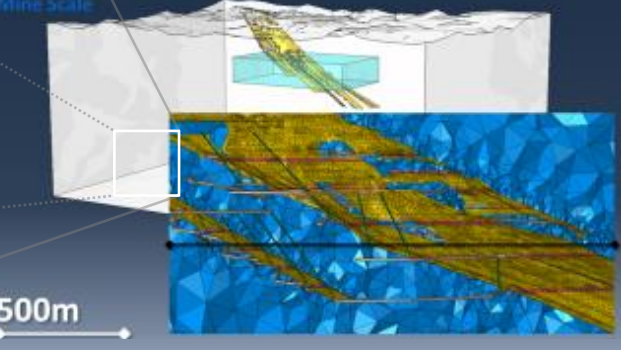
5m



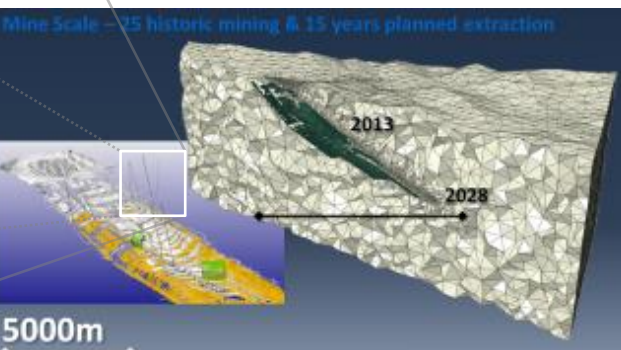
50m



500m



5000m



Acknowledgement:



<http://www.powersof10.com>

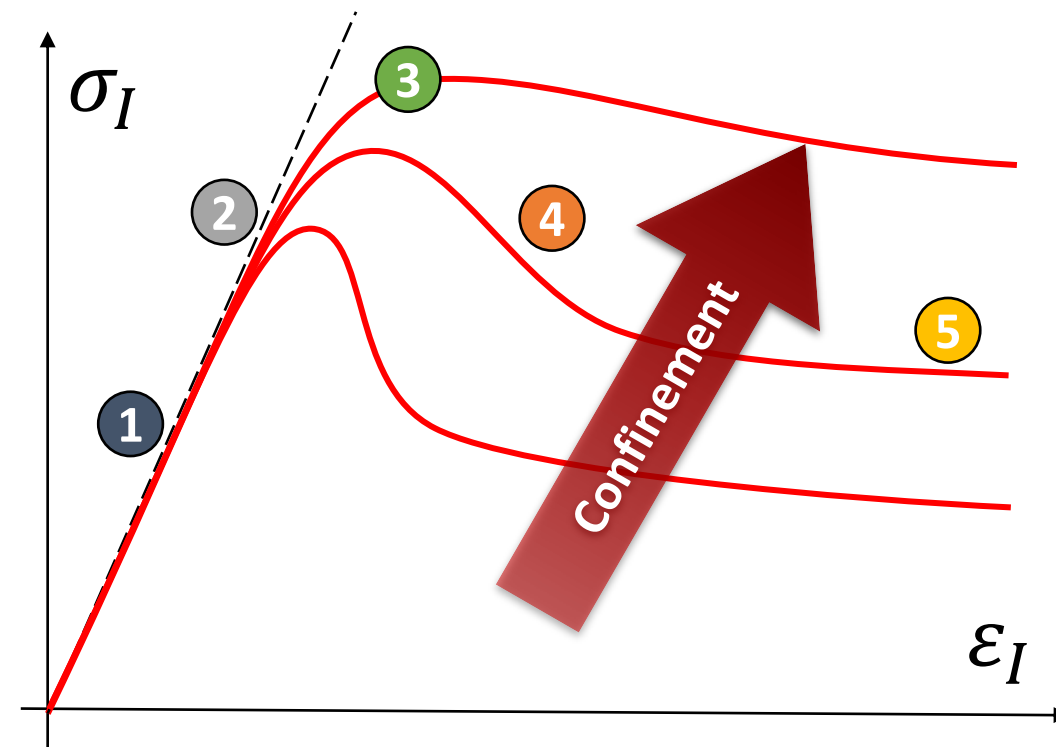
Simulation

Modelling Rock Mass in High Stress: IUCM – Rock Anisotropy in Constitutive Models

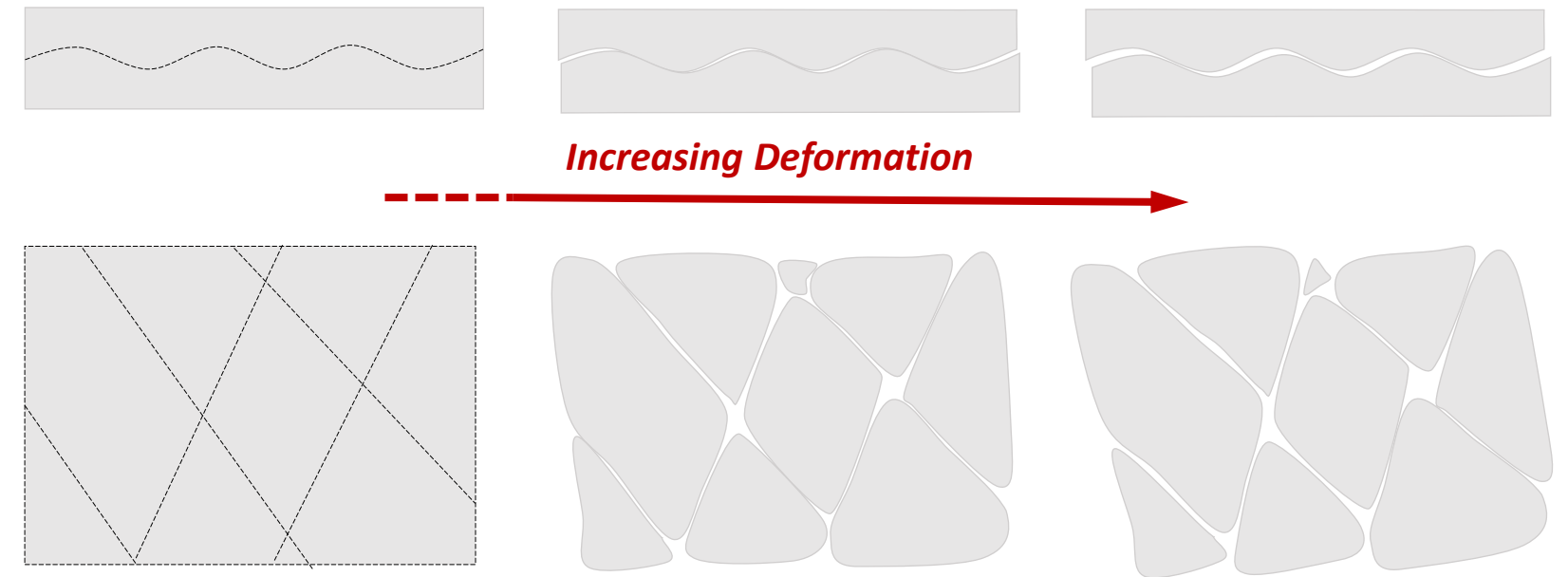
Modelling Rock Mass in High Stress: IUUCM

Stress – Strain

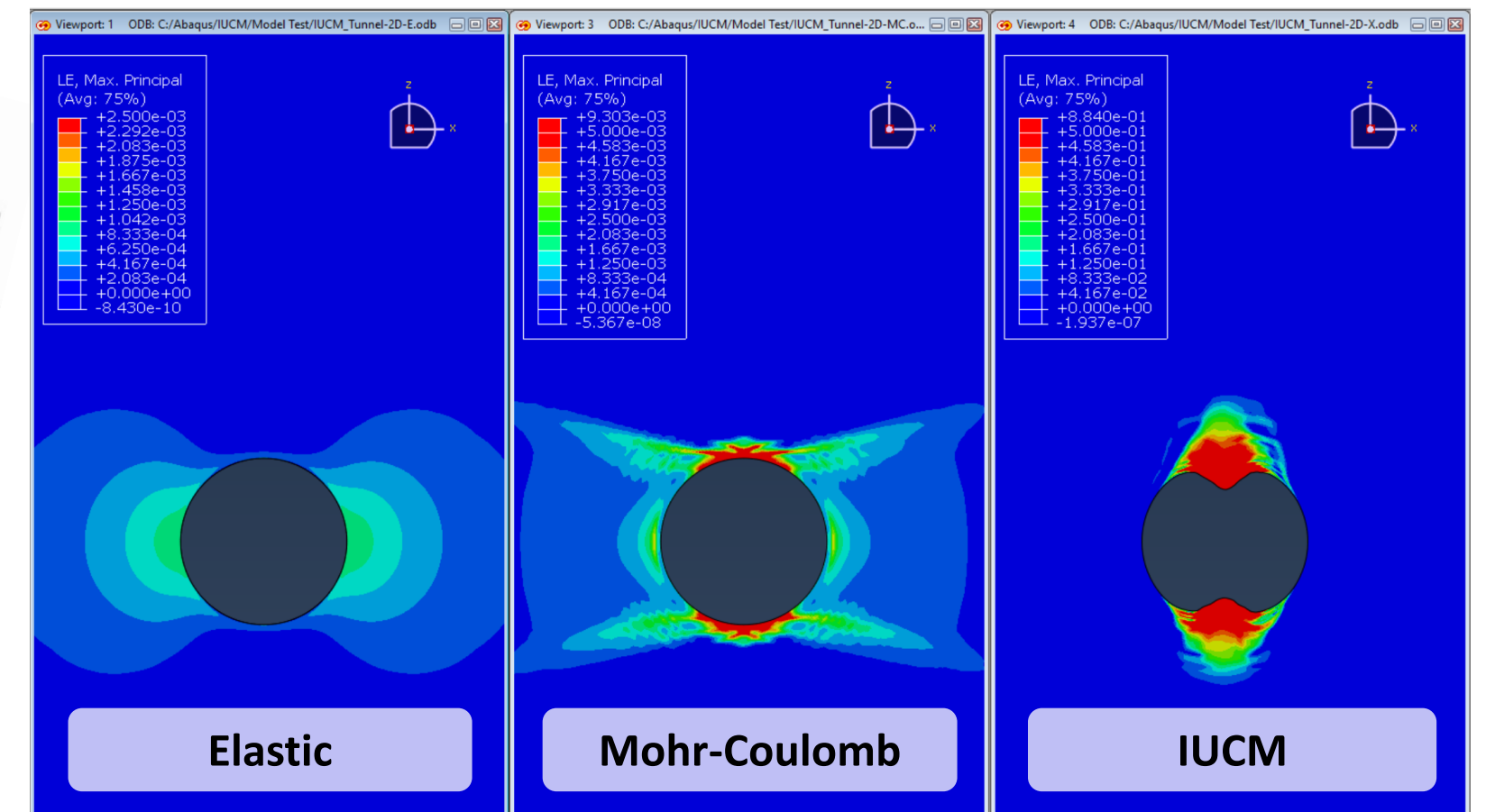
- 1) Elastic
- 2) Fracturing (onset of in-elastic behaviour)
- 3) Peak strength
- 4) Softening
- 5) Broken (residual strength)



Dilation



IUCM

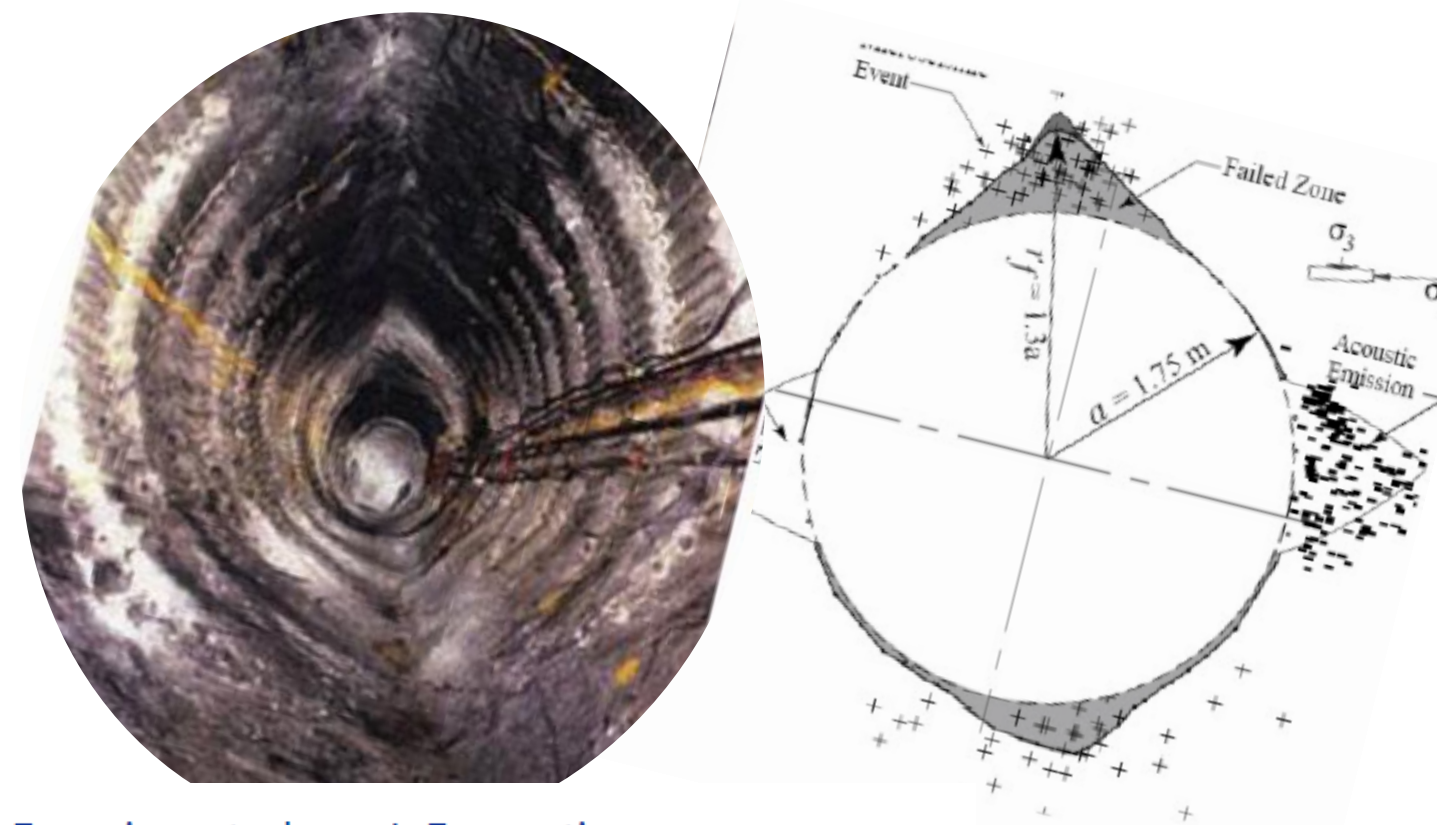


Mine-by-experiment

Cai et al. (2004)

Hajiabdolmajid et al. (2002)

Read, Martin (1996)

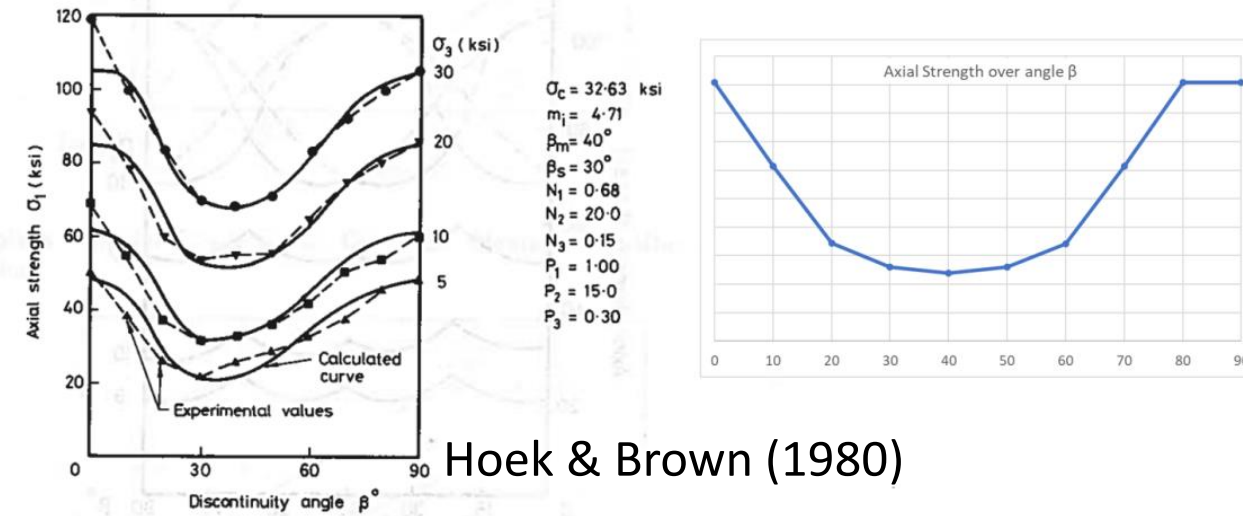
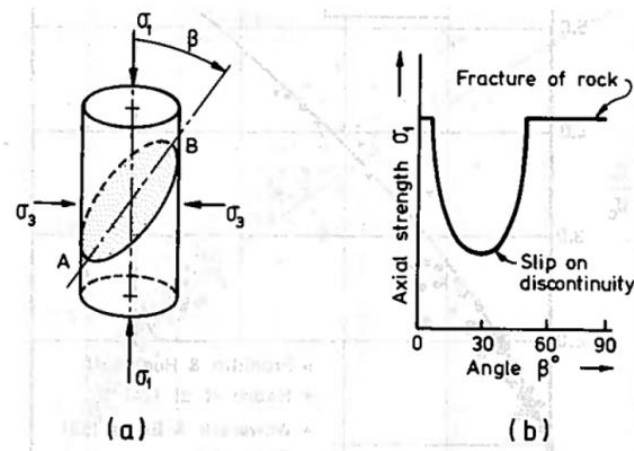


PDF [Technical summary of AECL's Mine-by Experiment phase I: Excavation response](#)
 Read, R.S.; Martin, C.D. (Atomic Energy of Canada Ltd., Pinawa, MB (Canada). Whiteshell Labs.)

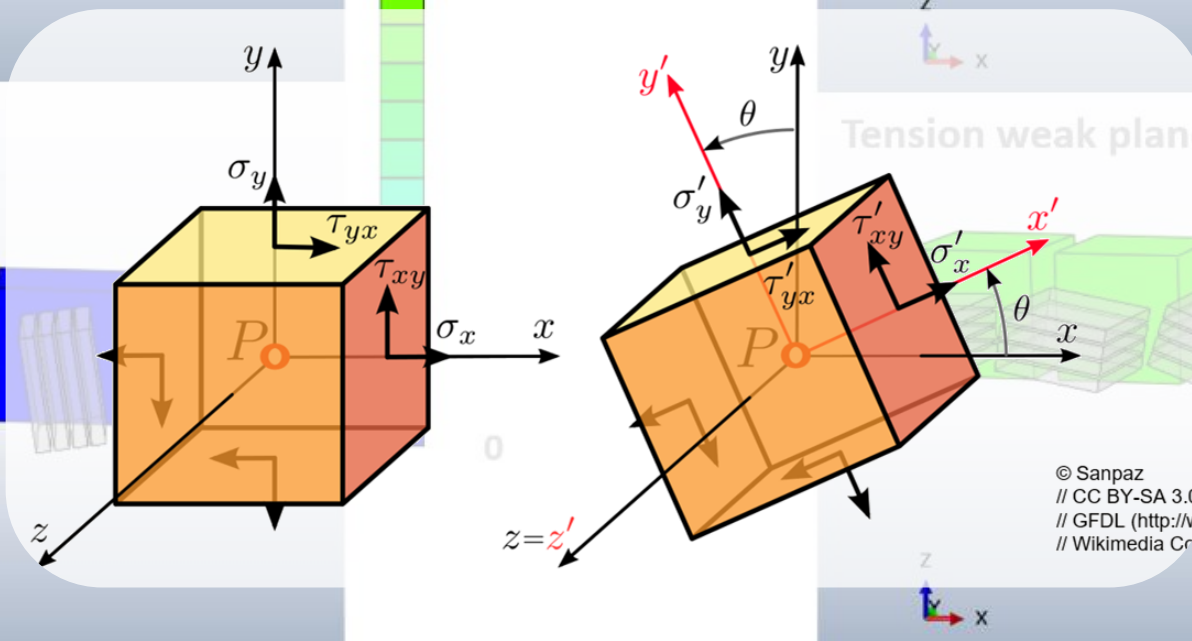
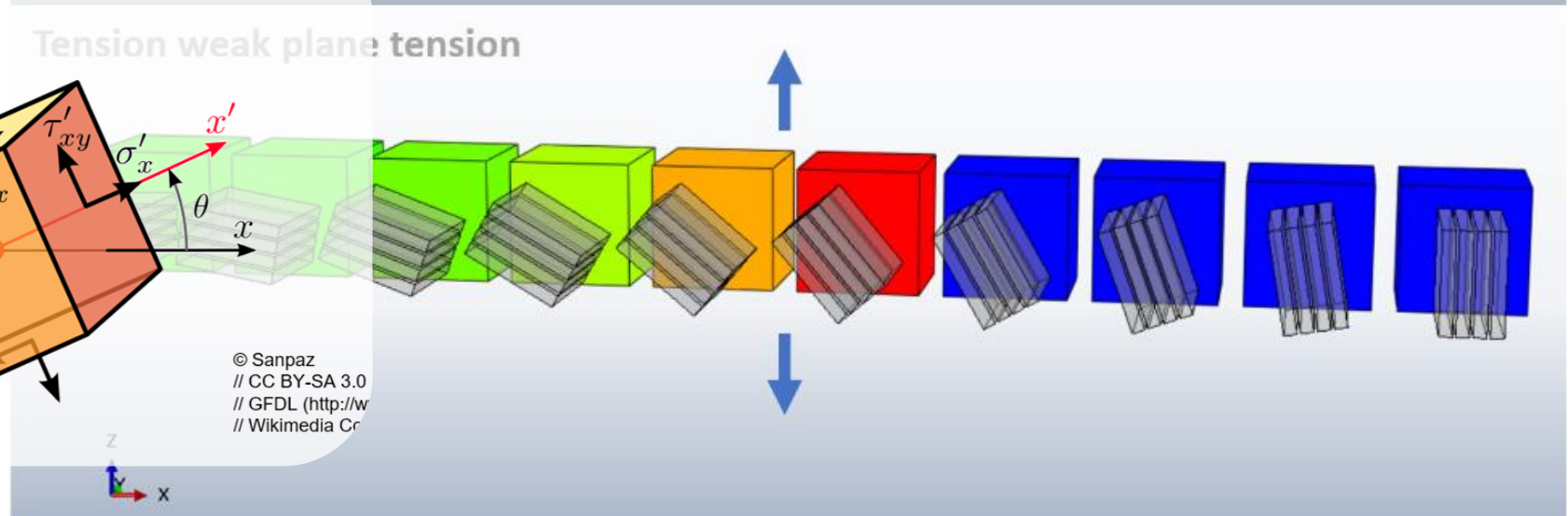
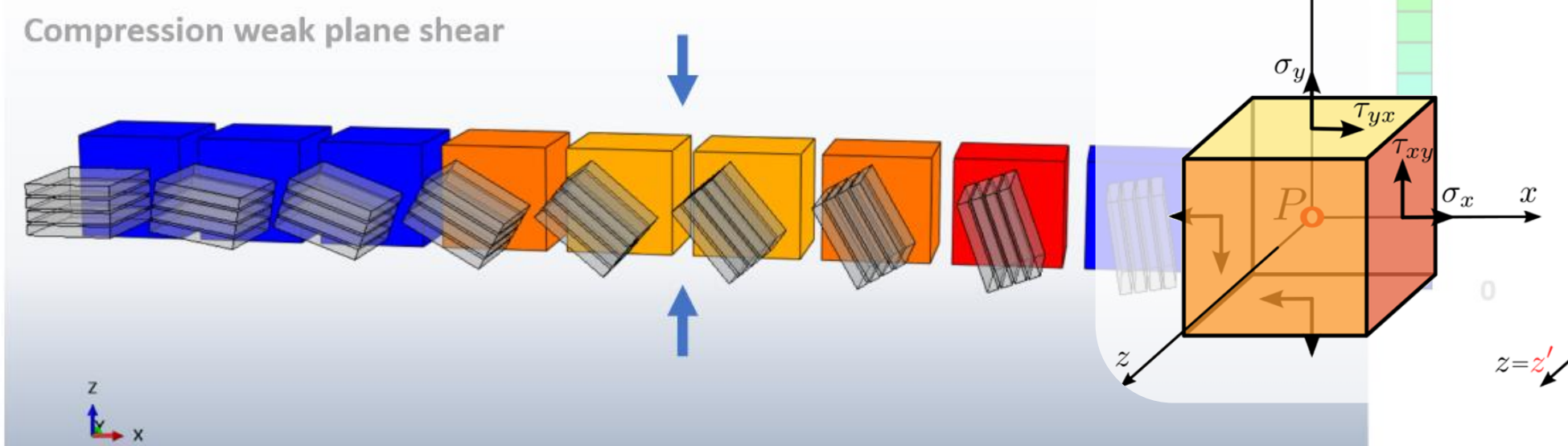
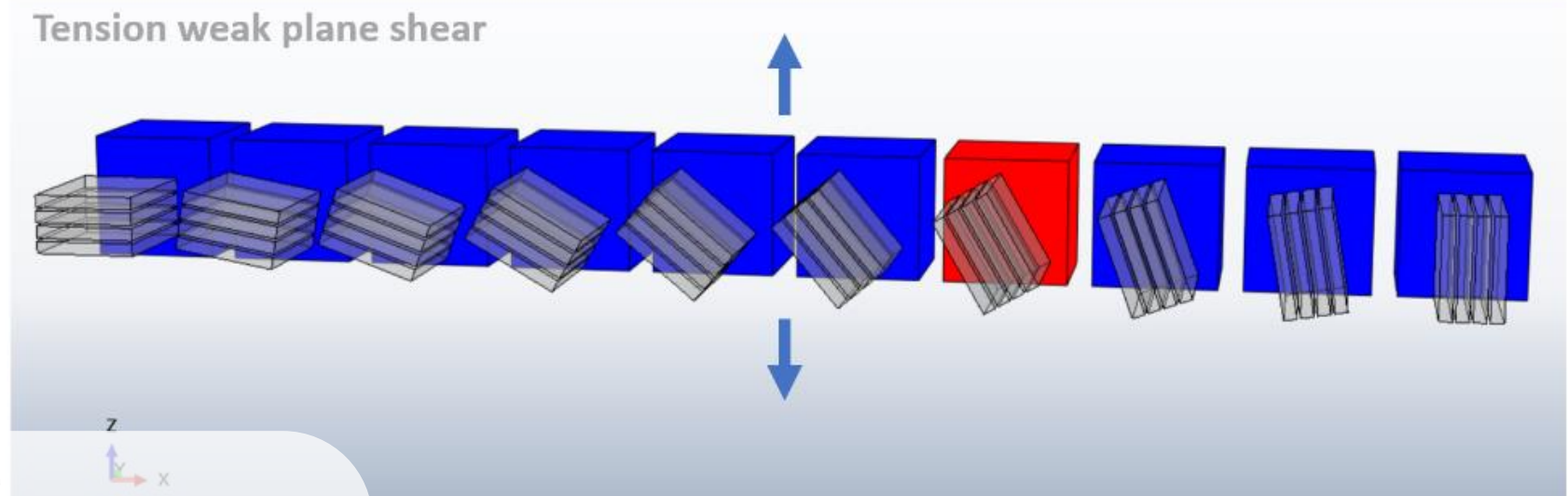
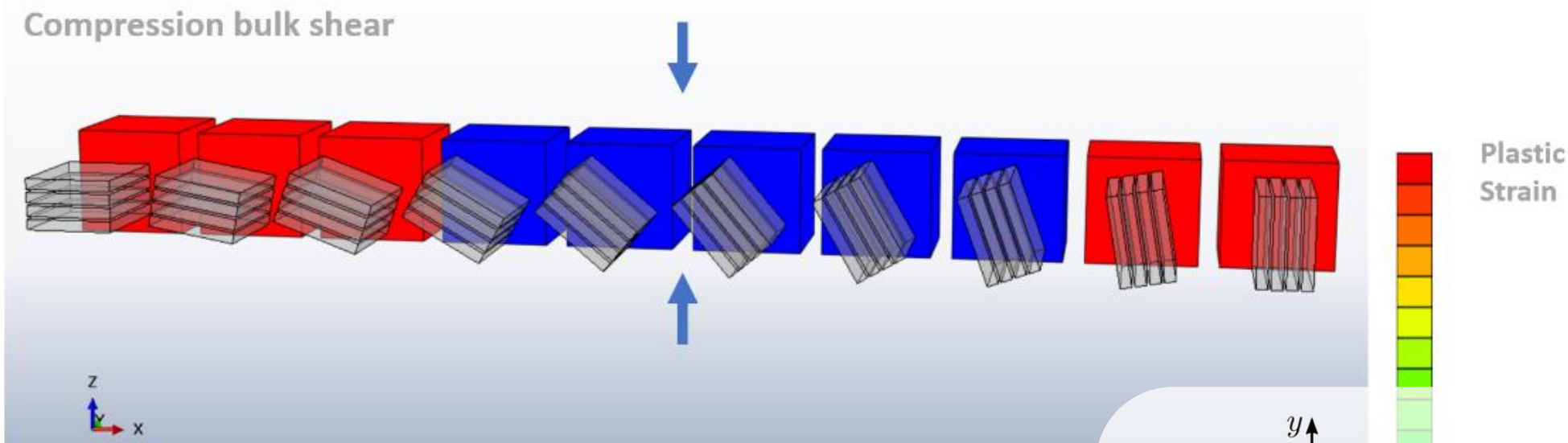
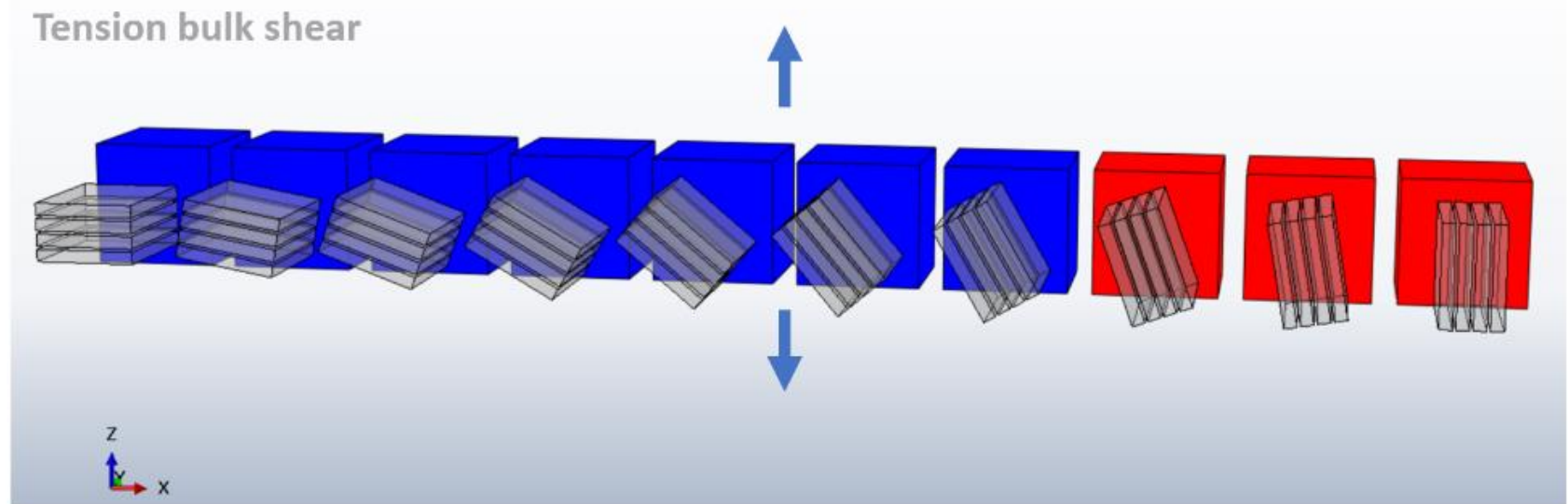
Atomic Energy of Canada Ltd., Pinawa, MB (Canada). Whiteshell Labs

1996

Rock Anisotropy in Constitutive Models



Hoek & Brown (1980)



© Sanpaz
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 // GFDL (http://w
 // Wikimedia Cr

Improved Unified Constitutive Model – IUCM

IUCM Features (Vakili 2016)

- *Non-linear Hoek-Brown*
- *Brittle to ductile transition*
- *Confinement-dependent strain-softening*
- *Non-linear evolution of dilation*
- *Elastic stiffness softening*
- *Strength anisotropy (weak plane)*
- *Available as a constitutive model library (VUMAT) for Abaqus / Simulation Manager*

1. Initialise the pre-mining stresses in the model.
2. Obtain the current minor and major principal stresses for each finite difference zone (or element in the finite element method).
3. Obtain minor principal stress increment ($\Delta\sigma_3$) by adding and subtracting 0.1% of the current σ_3 magnitude,

$$\sigma_3^1 = \sigma_3 - 0.001\sigma_3 \quad (1)$$

$$\sigma_3^2 = \sigma_3 + 0.001\sigma_3 \quad (2)$$

4. Calculate constants for the Hoek-Brown criterion based on equations provided by Hoek et al. [35],

$$m_b = m_i \exp\left(\frac{GSI - 100}{28 - 14D}\right) \quad (3)$$

$$s = \exp\left(\frac{GSI - 100}{9 - 3D}\right) \quad (4)$$

$$a = \frac{1}{2} + \frac{1}{6} \left(e^{-\frac{GSI}{15}} + e^{-\frac{D}{3}} \right) \quad (5)$$

5. Obtain the major principal stress increment ($\Delta\sigma_1$) from the generalised Hoek-Brown failure criterion [35] and from the measured change in the minor principal stress ($\Delta\sigma_3$),

$$\sigma_1^1 = \sigma_3^1 - \sigma_c \left(m_b \frac{\sigma_3^1}{\sigma_c} + s \right)^a \quad (6)$$

$$\sigma_1^2 = \sigma_3^2 - \sigma_c \left(m_b \frac{\sigma_3^2}{\sigma_c} + s \right)^a \quad (7)$$

6. Obtain the slope (ψ) of the incremental stress envelope,

$$\tan \psi = \frac{\sigma_1^1 - \sigma_1^2}{\sigma_3^1 - \sigma_3^2} \quad (8)$$

7. Calculate instantaneous friction angle (ϕ) from ψ ,

$$\phi = \sin^{-1} \left(\frac{\tan \psi - 1}{\tan \psi + 1} \right) \quad (9)$$

8. Calculate instantaneous cohesion,

$$c = \frac{\sigma_1^1(1 - \sin \phi) - \sigma_3^1(1 + \sin \phi)}{2 \cos \phi} \quad (10)$$

9. Calculate uniaxial tensile strength,

$$\sigma_t = \frac{s\sigma_c}{m_b} \quad (11)$$

10. To avoid the corresponding comparison, compare the maximum value and the maximum value.

Computers and
Geotechnics

(Vakili 2016)

```
// IUCM (Vakili, 2016)
// -----
// 3: sigma3 variation (dS = +/- 0.001) - formulas use [MPa] (!)
dS3_1 = abs(0.999 * eigVal[3]) / c_1MPa;
dS3_2 = abs(1.001 * eigVal[3]) / c_1MPa;

// 4: Hoek-Brown constants
if (p_gsi > 99.9) prop_gsi = 99.9;
prop_hbmb = p_mimax * exp((prop_gsi - 100.) / (28. - 14. * p_disfac));
prop_hbs = exp((prop_gsi - 100.) / (9. - 3. * p_disfac));
prop_hba = 0.5 + 1. / 6. * (exp(-prop_gsi / 15.) + exp(-20. / 3.));

// 5: generalised Hoek-Brown failure criterion
dS1_1 = dS3_1 + p_sigci * pow(prop_hbmb * (dS3_1 / p_sigci) + prop_hbs, prop_hba);
dS1_2 = dS3_2 + p_sigci * pow(prop_hbmb * (dS3_2 / p_sigci) + prop_hbs, prop_hba);

// 6: slope of HB curve, current friction & cohesion
dS_tanPsi = (dS1_2 - dS1_1) / (dS3_2 - dS3_1);

// 7: instantaneous friction angle
prop_phi = asin((dS_tanPsi - 1.) / (dS_tanPsi + 1.));

// 8: instantaneous cohesion
dS_sinPhi = sin(prop_phi);
prop_coh = (dS1_1 * (1. - dS_sinPhi) - dS3_1 * (1. + dS_sinPhi)) / (2. * cos(prop_phi));

// 9: uniaxial tensile strength
prop_ten = prop_hbs * p_sigci / prop_hbmb;

// 10: maximum tensile strength & bracket friction angle (ap
if (prop_phi <= c_minA) prop_phi = c_minA;
if (prop_phi >= c_maxA) prop_phi = c_maxA;

s_tmax = prop_coh / tan(prop_phi);
if (prop_ten > s_tmax) prop_ten = s_tmax;
```

Abaqus User
Subroutine

“What you see is what you get”



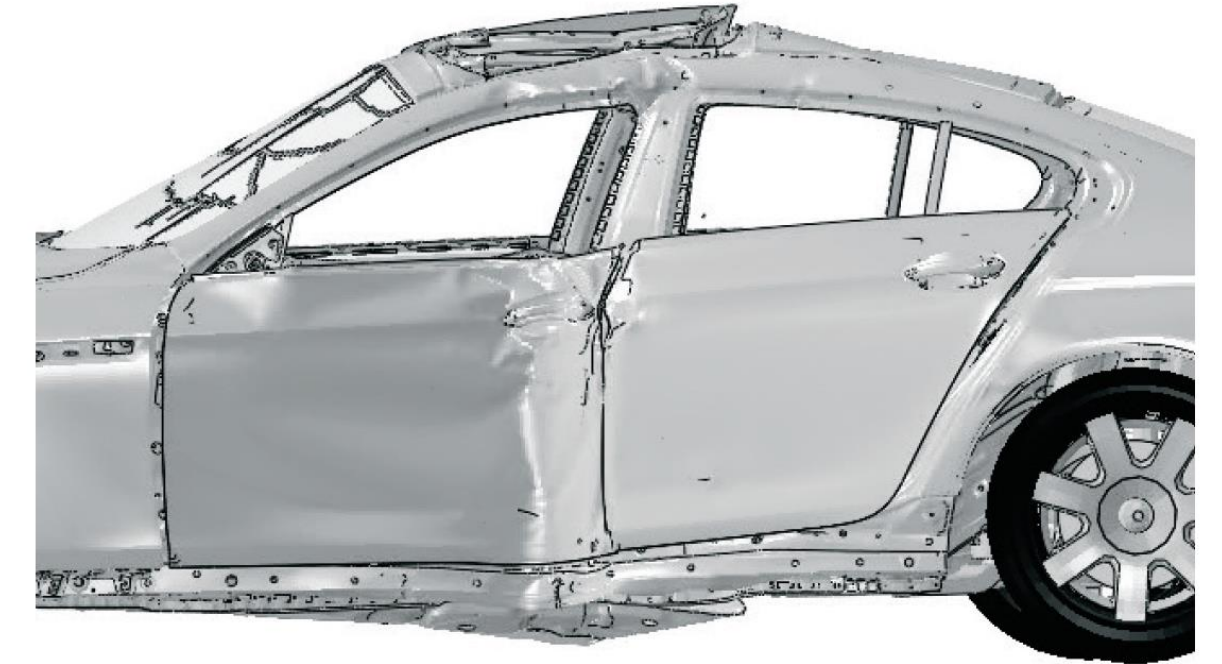
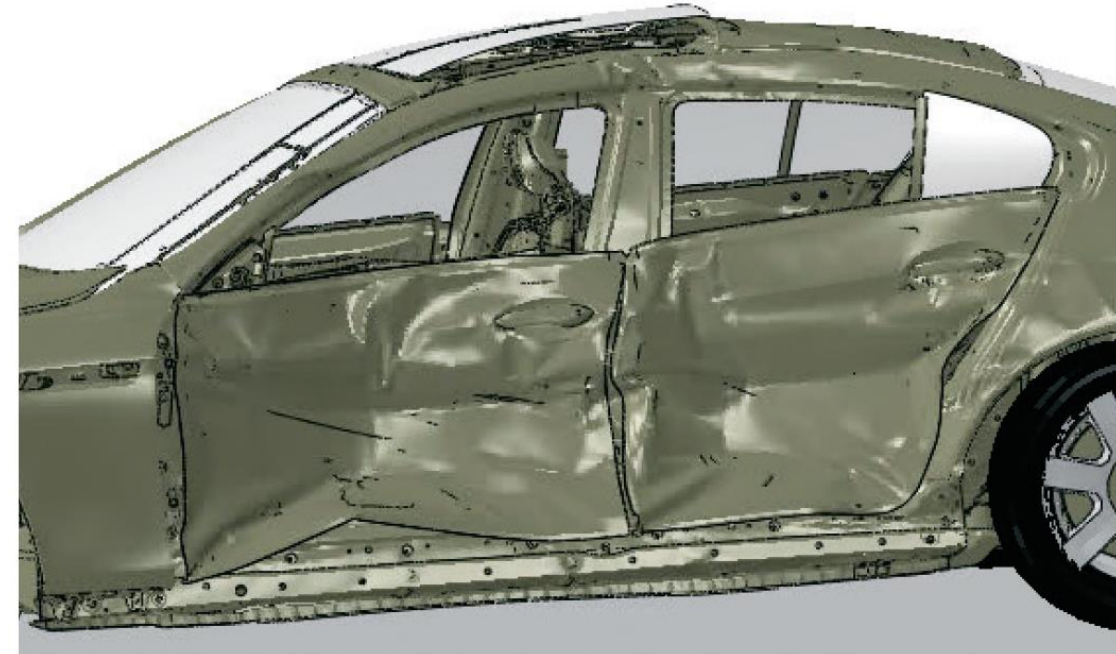
Zero Prototypes

Zero Prototypes

DS DASSAULT
SYSTEMES

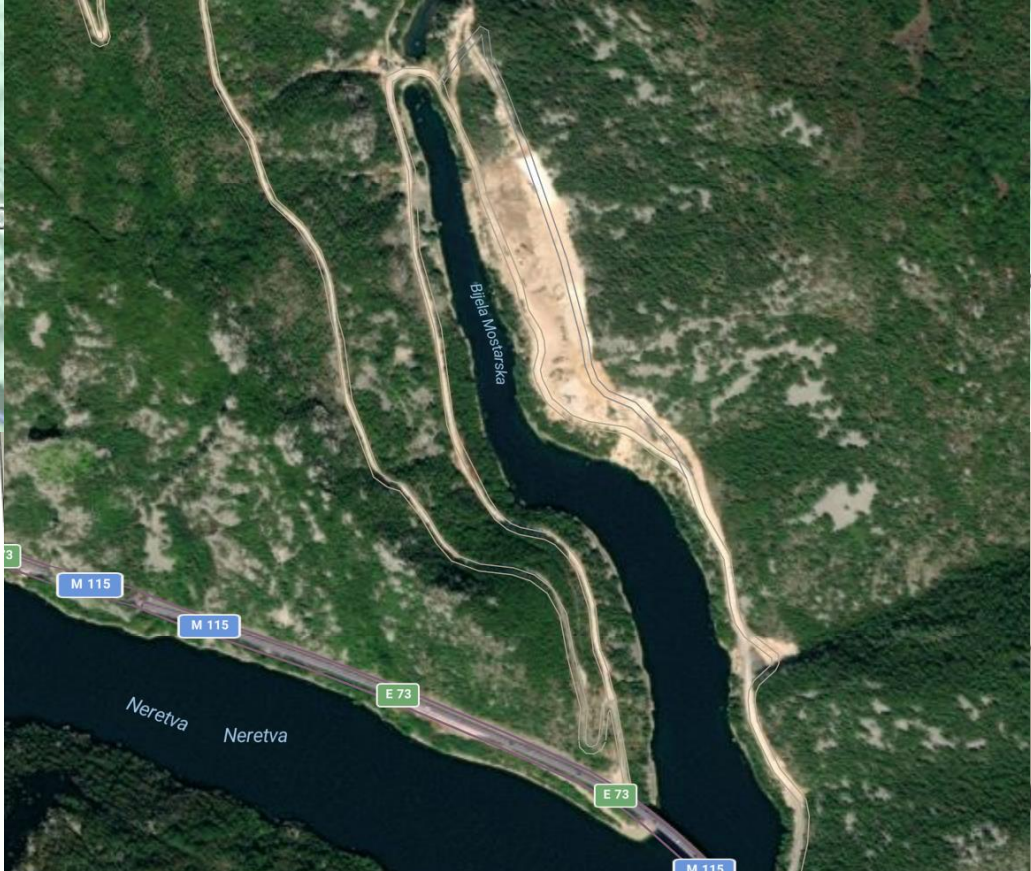
DS SIMULIA

**MOVING TOWARDS ZERO-PROTOTYPING
FOR AUTOMOTIVE PASSIVE SAFETY**



Courtesy BMW/SIMULIA

Real World 'Prototypes'



Workflows

Slope Stability – Solution Pathway – Pore Pressure – Underground Workflows –
StopeX and SlopeX

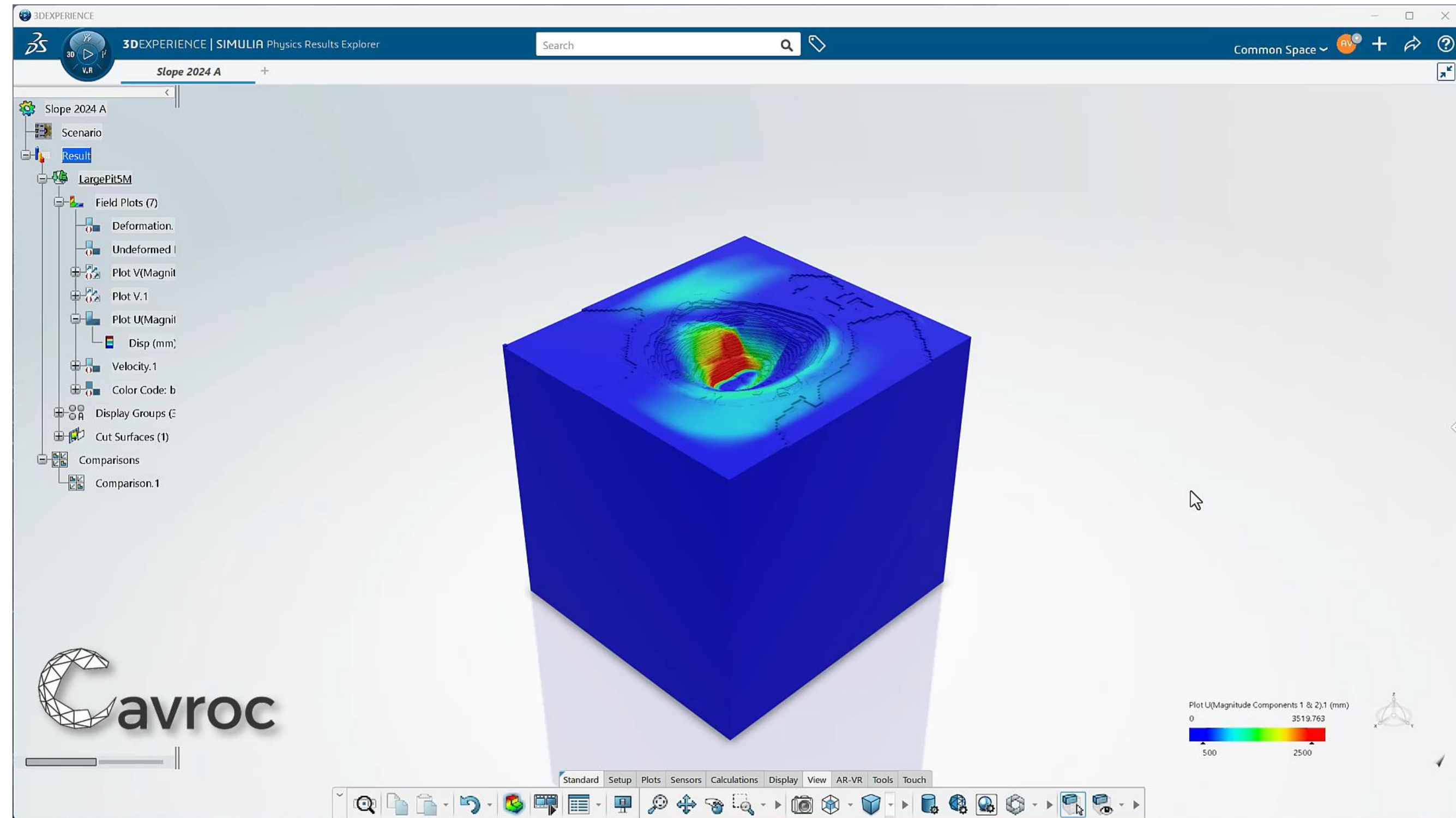
Slope Stability

Stability analysis is a central element of the slope design process*

- **Safety** (zero harm & protecting the environment)
- **Project economics & reducing financial risk**
- **Sustainability** (energy consumption, waste)

Accurate 3D Numerical Modelling can contribute significantly to these objectives.

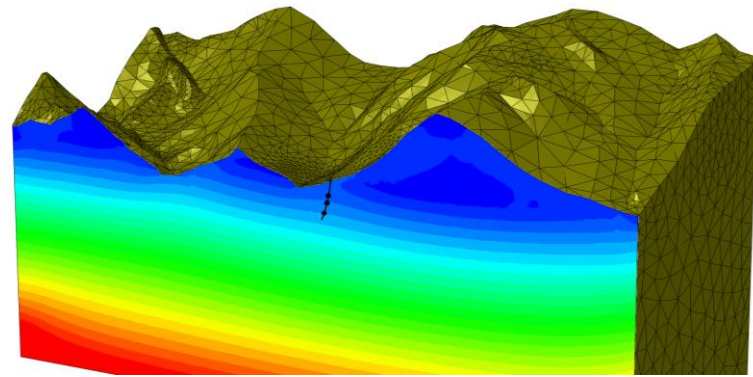
* "Guidelines for Open Pit Slope Design", Read (Ed.) 2009. CSIRO Publishing.



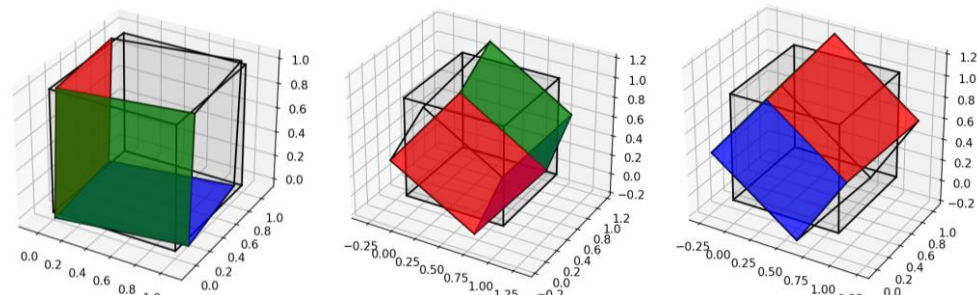
Tectonic Stress and Model Equilibrium

There are many cases where no analytical solution for the initial condition of the stress field exists, requiring an equilibrium step:

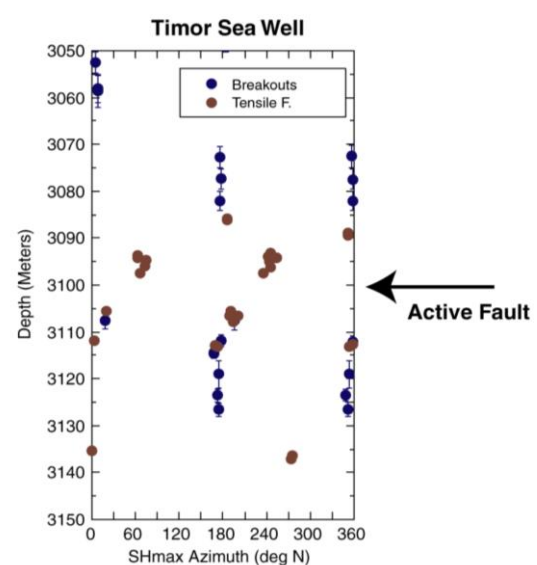
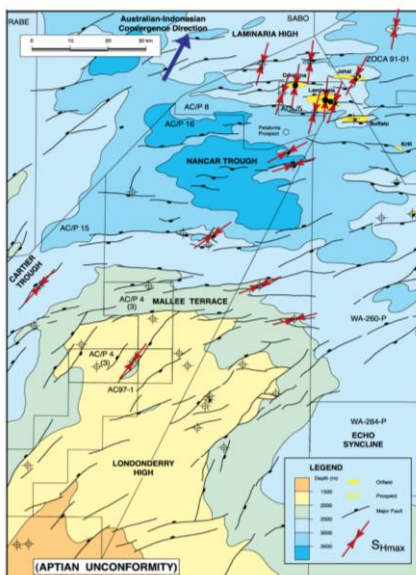
1) The model contains surface topography



2) The principal stress orientations are not horizontal and vertical



3) Locked in stress (faults, geology)



Abaqus 2024

Date 07-Feb-2024 Time 13:54:42

PROBLEM SIZE

NUMBER OF ELEMENTS IS 3038020
 NUMBER OF NODES IS 3601025
 TOTAL NUMBER OF VARIABLES IN THE MODEL 10803075

4 CPUs

10M DoF

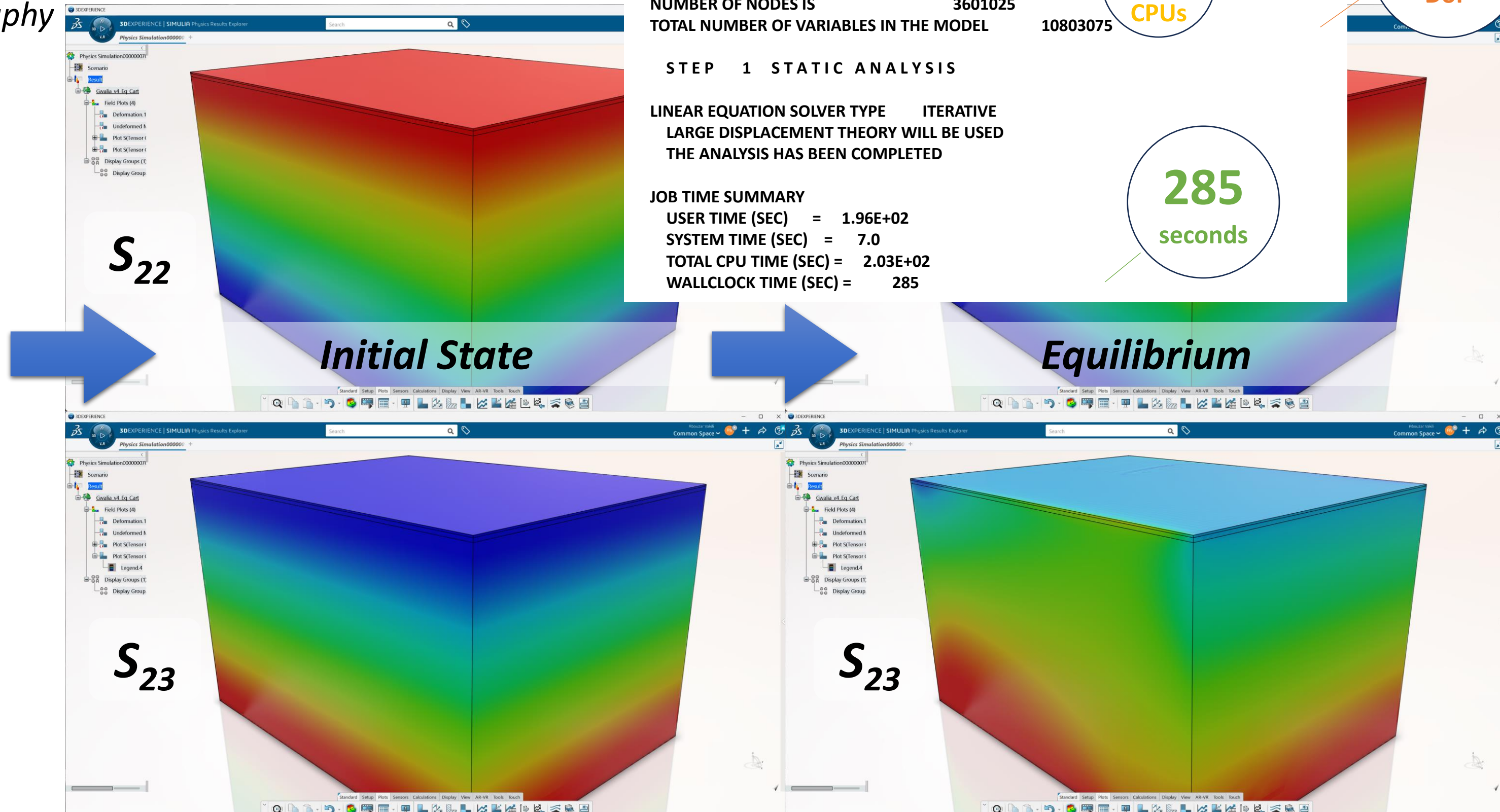
STEP 1 STATIC ANALYSIS

LINEAR EQUATION SOLVER TYPE ITERATIVE
 LARGE DISPLACEMENT THEORY WILL BE USED
 THE ANALYSIS HAS BEEN COMPLETED

JOB TIME SUMMARY

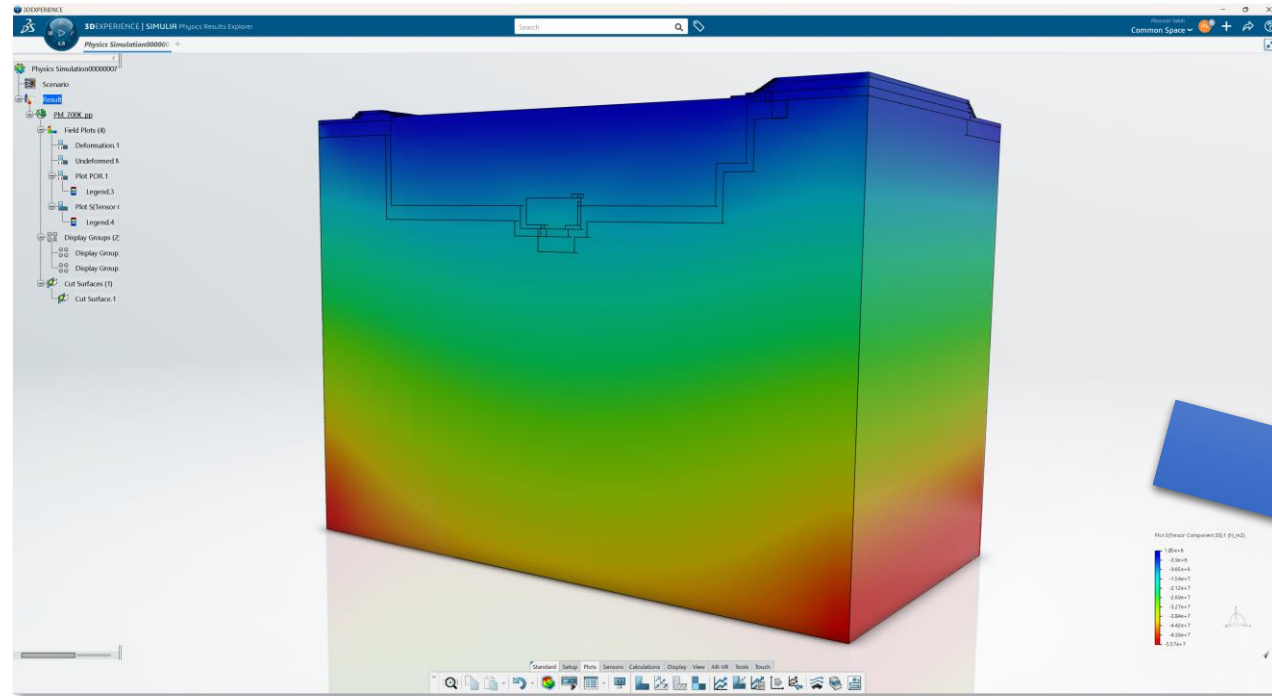
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 SYSTEM TIME (SEC) = 7.0
 TOTAL CPU TIME (SEC) = 2.03E+02
 WALLCLOCK TIME (SEC) = 285

285 seconds

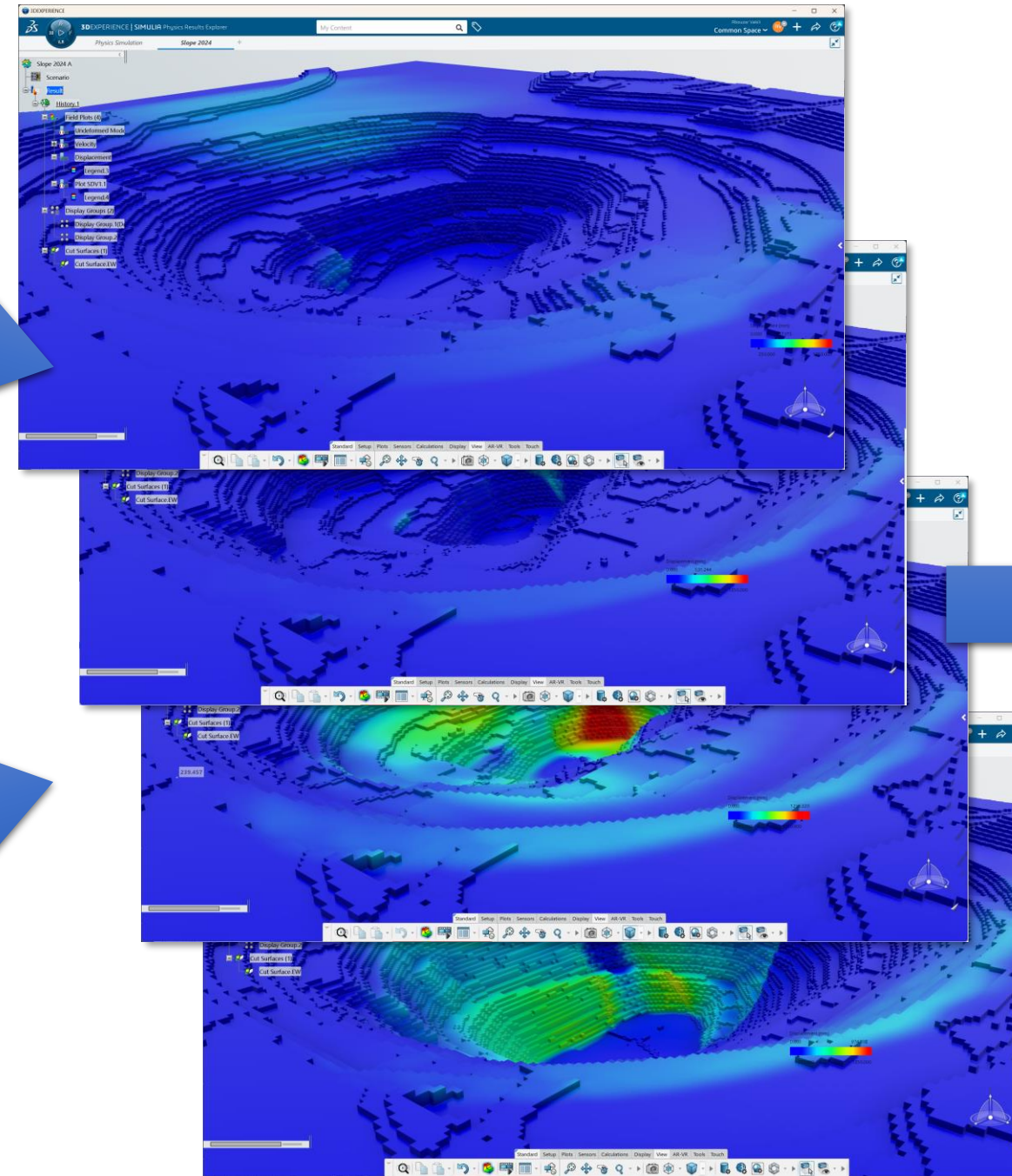


Solution Pathway: Equilibrium to Instability

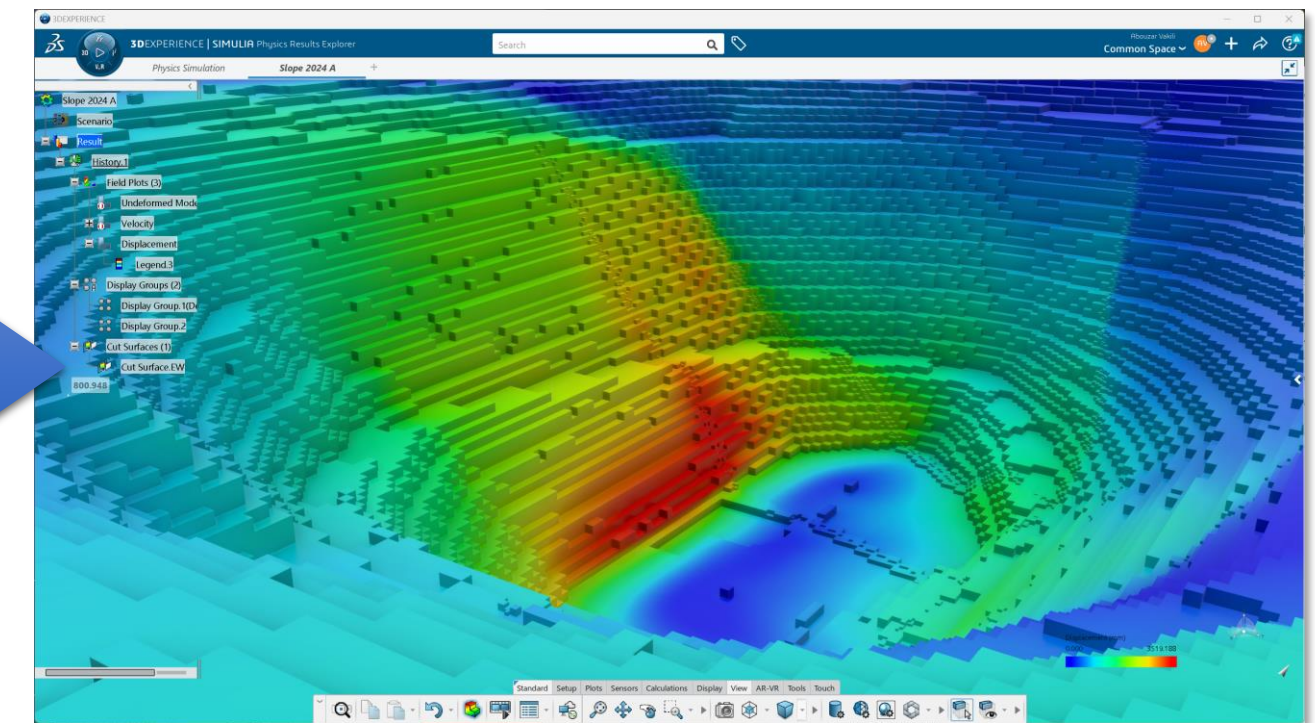
Initial Stress & Equilibrium



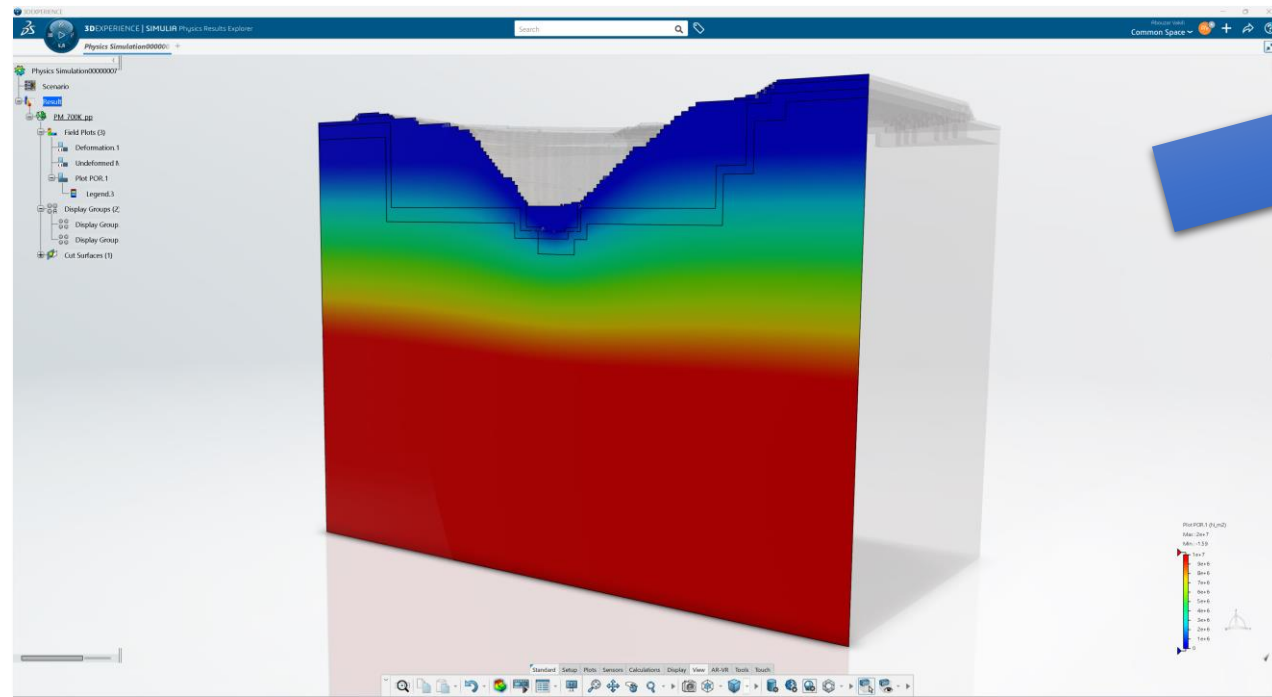
Pit Excavation Sequence



Shear Strength Reduction



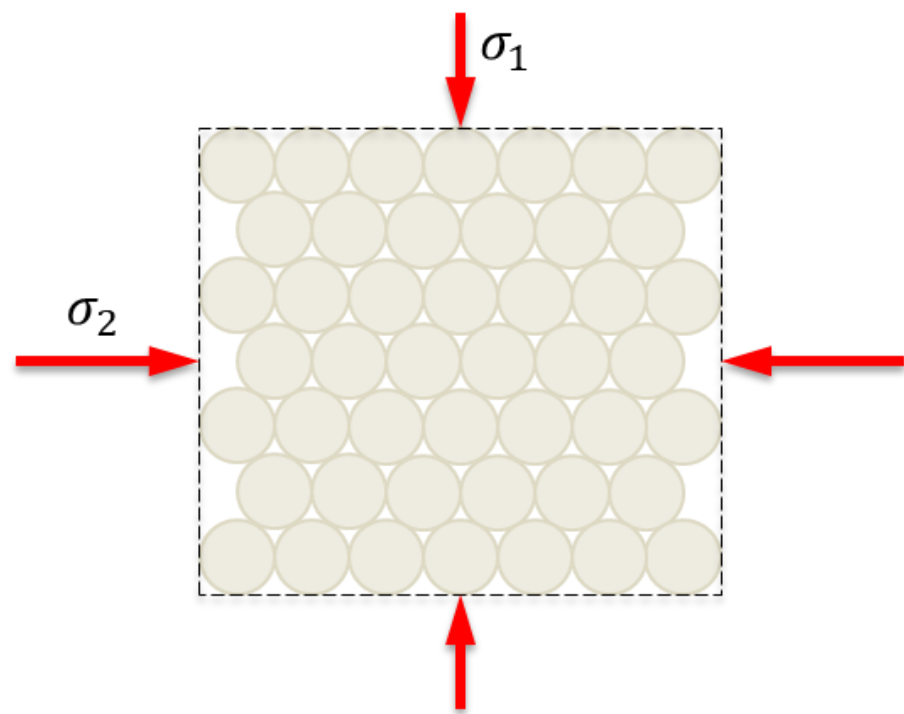
Pore Pressure(s)



Pore Pressure

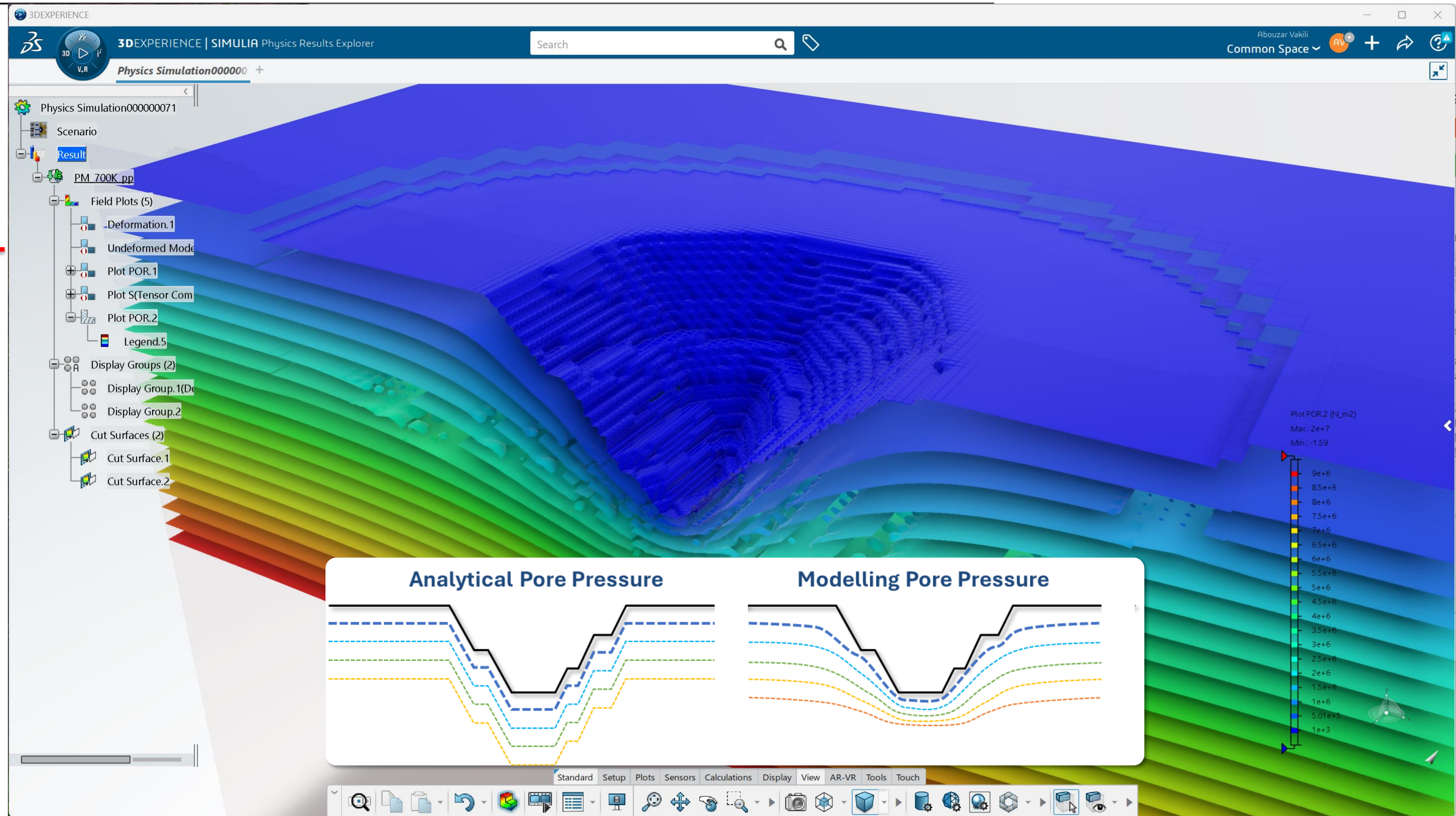
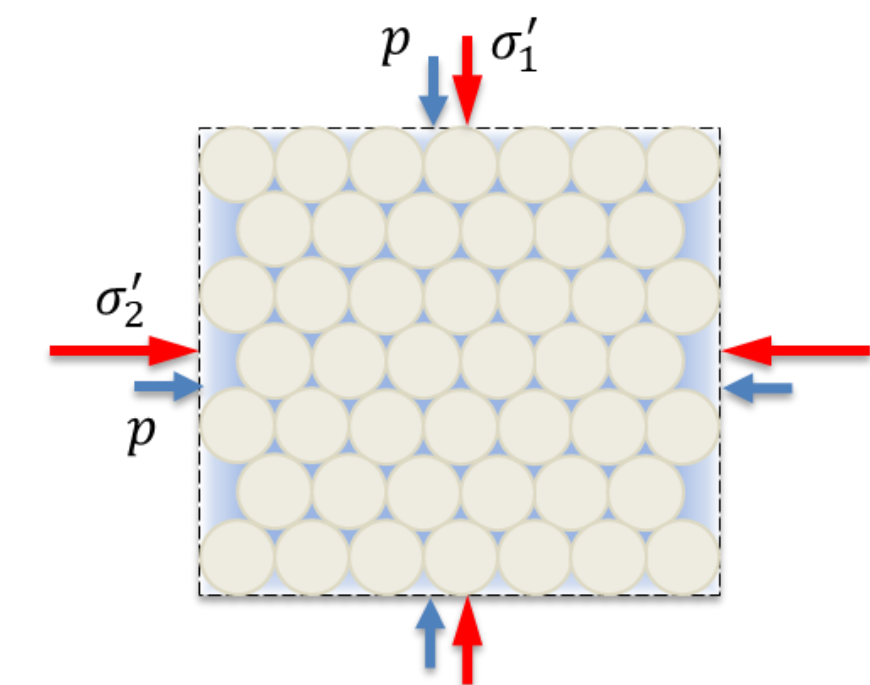
Dry Medium

Stress acting on the matrix



Saturated Medium

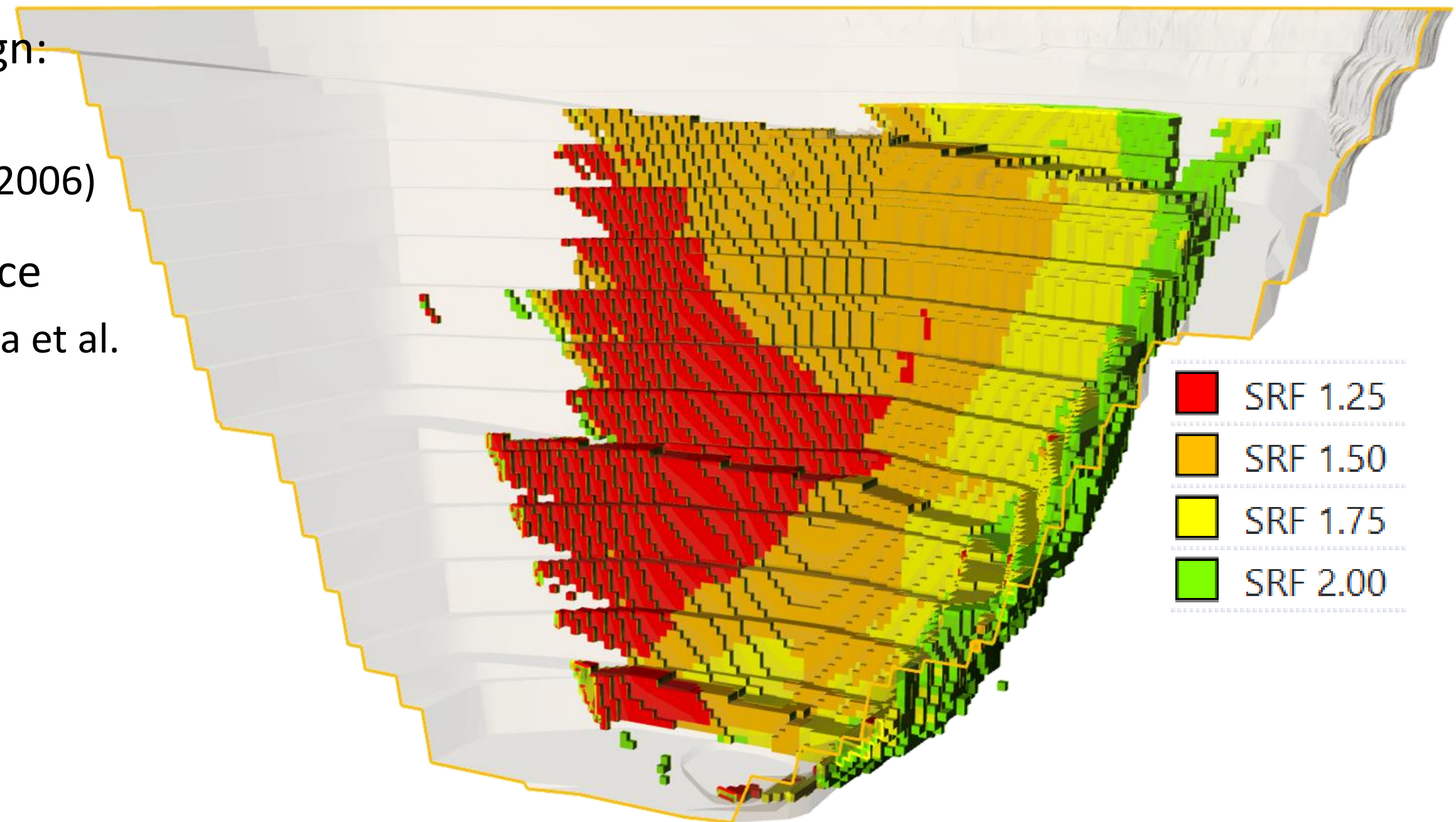
Stress acting on matrix and fluid



Reliability-Based Design Access Criteria

Reliability-Based Design Access Criteria (RBDAC)

- **Failure volume and location** are required inputs for the economic risk assessment of inter-ramp & overall pit slope designs (Creighton et al. 2022)
- Risk-consequence approach to open pit slope design: *“Risk criteria are therefore set on the basis of consequences of potential failures”* (Terbrugge et al. 2006)
- Consider design acceptance criteria using confidence classification and consequence categories (Macciotta et al. 2020)



Underground Workflow

- Mine Geometry
- Geology & Faults
- Extraction Sequence
- In-situ Stress
- Rock Mass Parameters



(not a real picture)



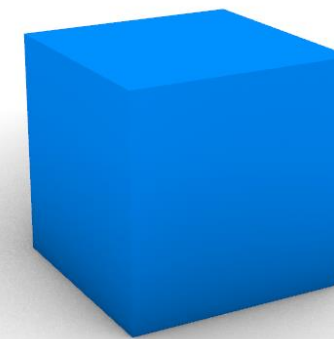
Cavroc StopeX

Abaqus/CAE
2024

Abaqus FEA

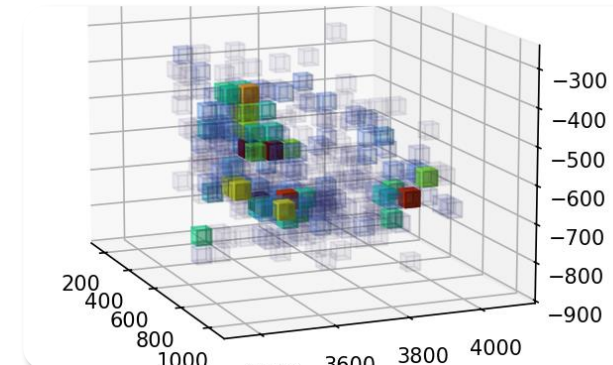
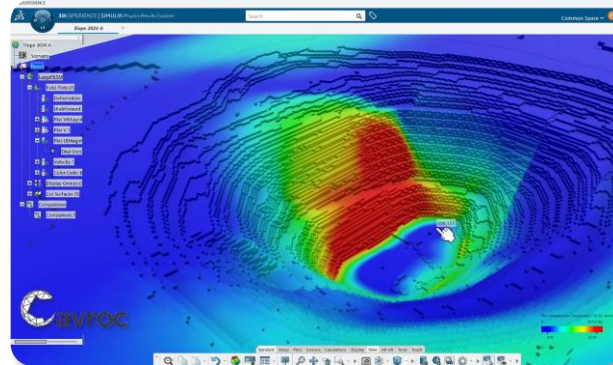
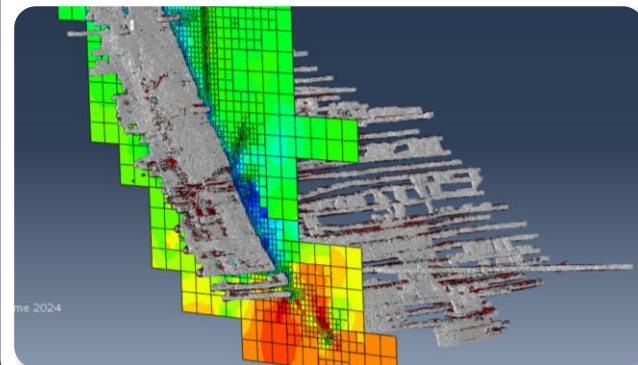


Simulation Manager

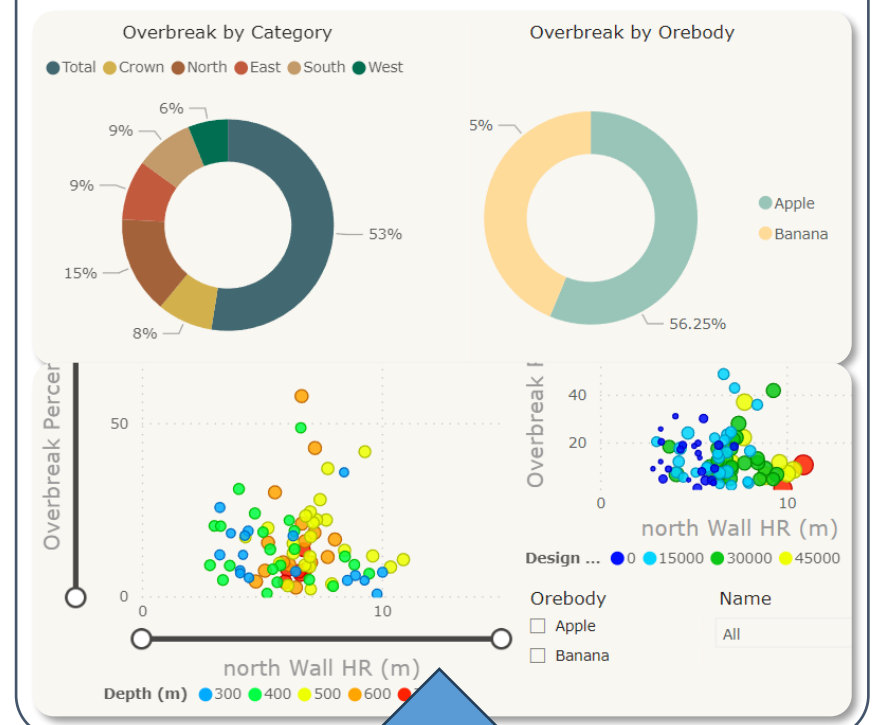


Other Solvers

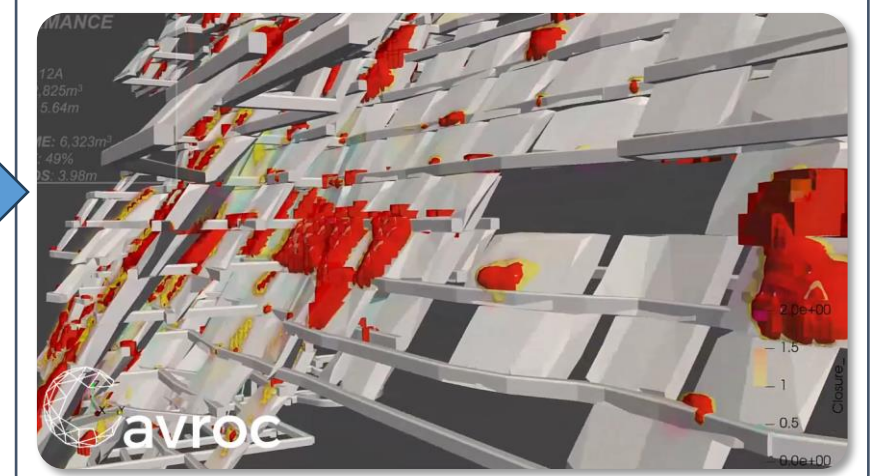
Visualisation & Results Processing (Python)



Dashboards

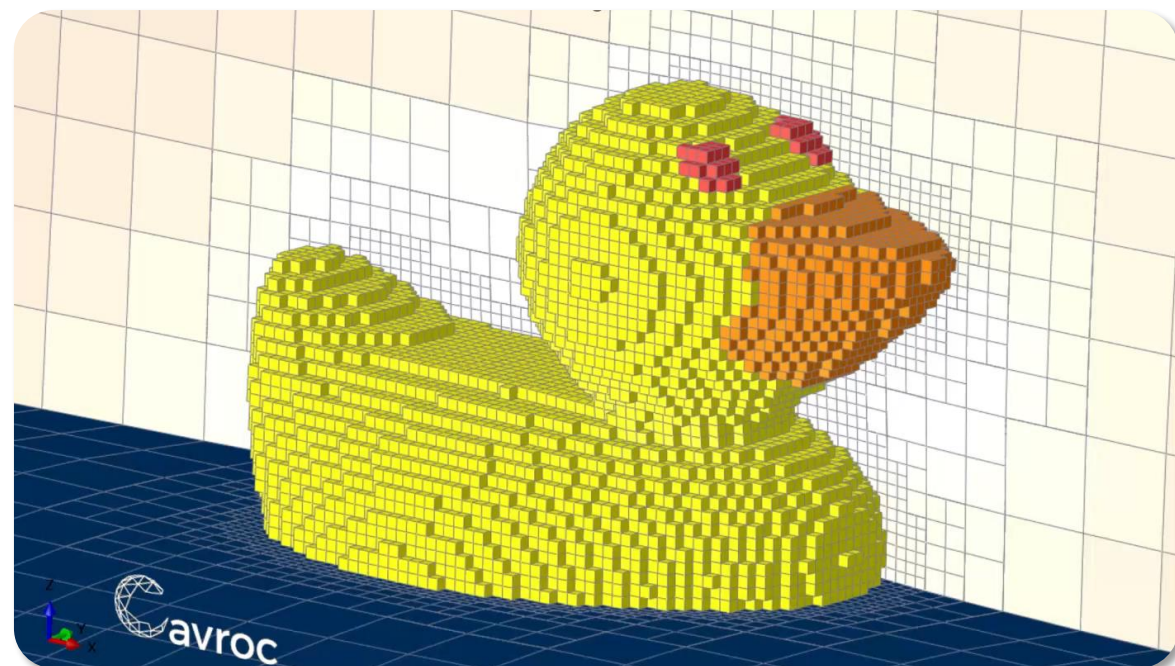


Cavroc RocboX



StopeX & SlopeX

- **Web-based** user interface
- **Rapid** model construction (~hours)
- Automated **octree** meshing
- Guided, best-practice, **workflows**
- Cavroc forum: **support & discussions**
- **IUCM** constitutive model for rock mass
- Supporting multiple **solvers**
- RocboX stope **performance** intelligence



A screenshot of the StopeX web interface. The browser address bar shows 'apps.cavroc.com/dashboard?v=modelconstruction&subnav=stopping'. The interface includes a sidebar with navigation options: Projects, Settings, Model Construction (highlighted), Rock Mass Domain, Faults, Backfill, Insitu Stress, and Solving Parameters. The main content area shows settings for 'Stopping', including 'Upload file from your computer' (with a file named 'stopes.stl'), 'Zone Densification Distance' (set to 10), 'Choose the relative geometry accuracy' (set to Intermediate), and 'Minimum Permissible Zone Size' (set to 1.5). There are also sections for 'Initial Zone Size' (set to 6) and a 'Save Model' button. The Cavroc logo is at the bottom center. A QR code and a 'SCAN ME' button are overlaid on the bottom right of the screenshot.

3DEXPERIENCE platform

Simulation Manager – Physics Results Explorer – Scalability – Virtual Reality

Simulation Manager

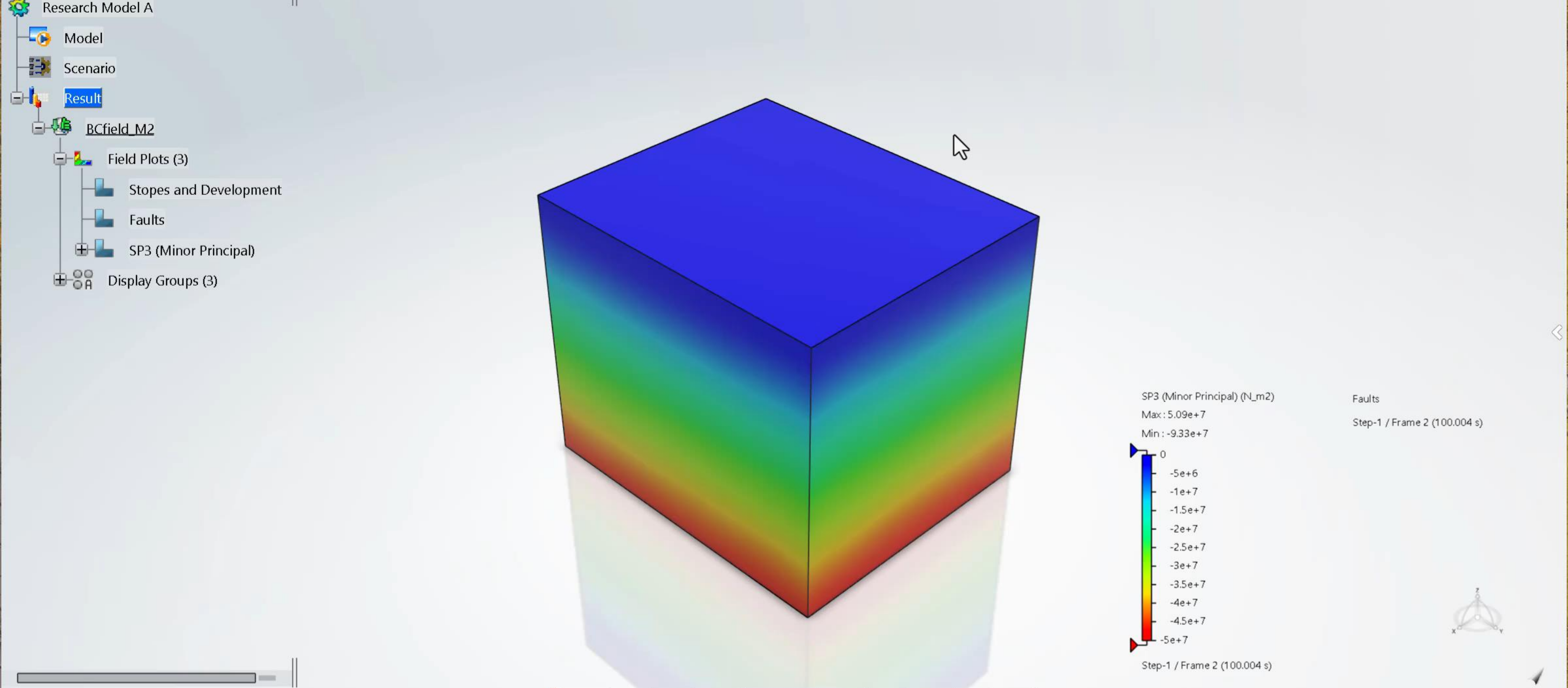
Title	Status	Results...	Ses...	Modification
-		41 GB		Sep 7, 2024,
-		32 GB		Sep 6, 2024,
-		4.62 GB		Sep 4, 2024,
-		4.63 GB		Aug 27, 2024,
-		9.42 GB		Aug 9, 2024,
-		AnalysisCase.2		Aug 9, 2024,
-		AnalysisCase.1		Aug 8, 2024,
-		SimuServ Diagnostics (A)		Jul 29, 2024,
-		AnalysisCase.2		Jul 29, 2024,
-		AnalysisCase.1		Jul 23, 2024,
-		SingleStope (A)		Jul 29, 2024,
-		Precompiled		Jul 29, 2024,
-		SourceCode		Jul 12, 2024,
-				Jul 19, 2024,
-				Aug 6, 2024,
-				Jul 19, 2024,
-				Jul 17, 2024,
-		Field Variable Test (A)		Jul 18, 2024,
-		Dip70.Direction70.FV.2024x.HF3		Jul 18, 2024,
-		Dip70.Direction70.FV		Dec 14, 2023,
-		WedgeFail_5M (A)		Apr 10, 2024,
-		AnalysisCase.1		Apr 10, 2024,

Storage: 56 GB

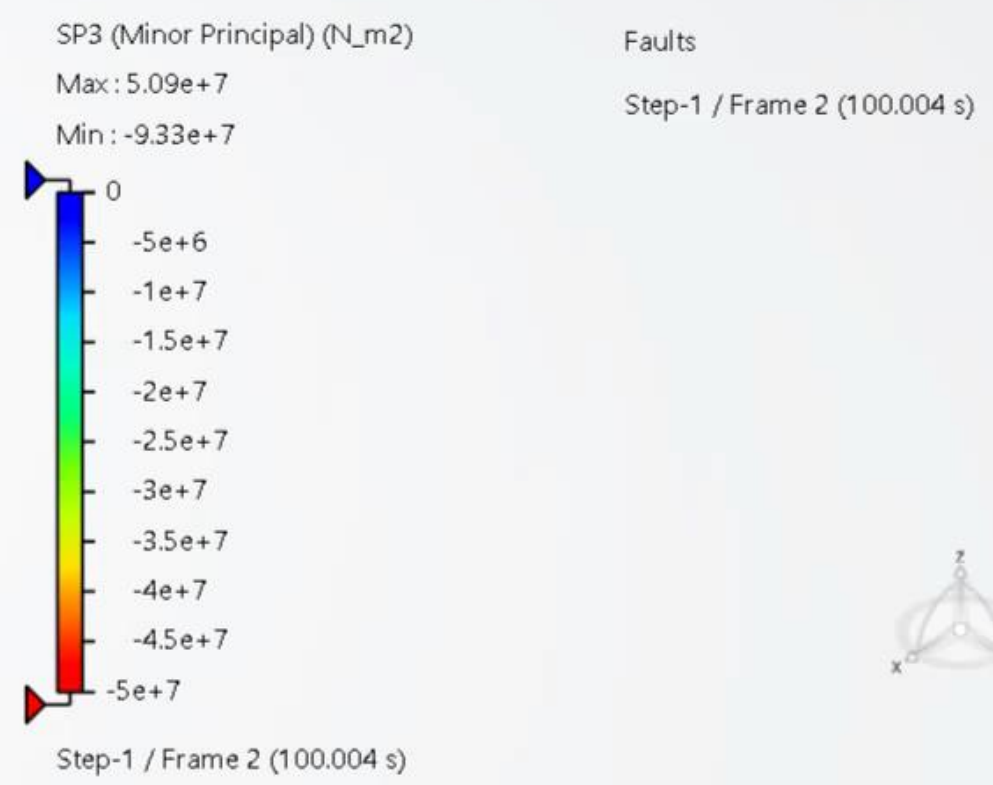
0 selected

Make a selection to view monitoring details or set up and run a simulation

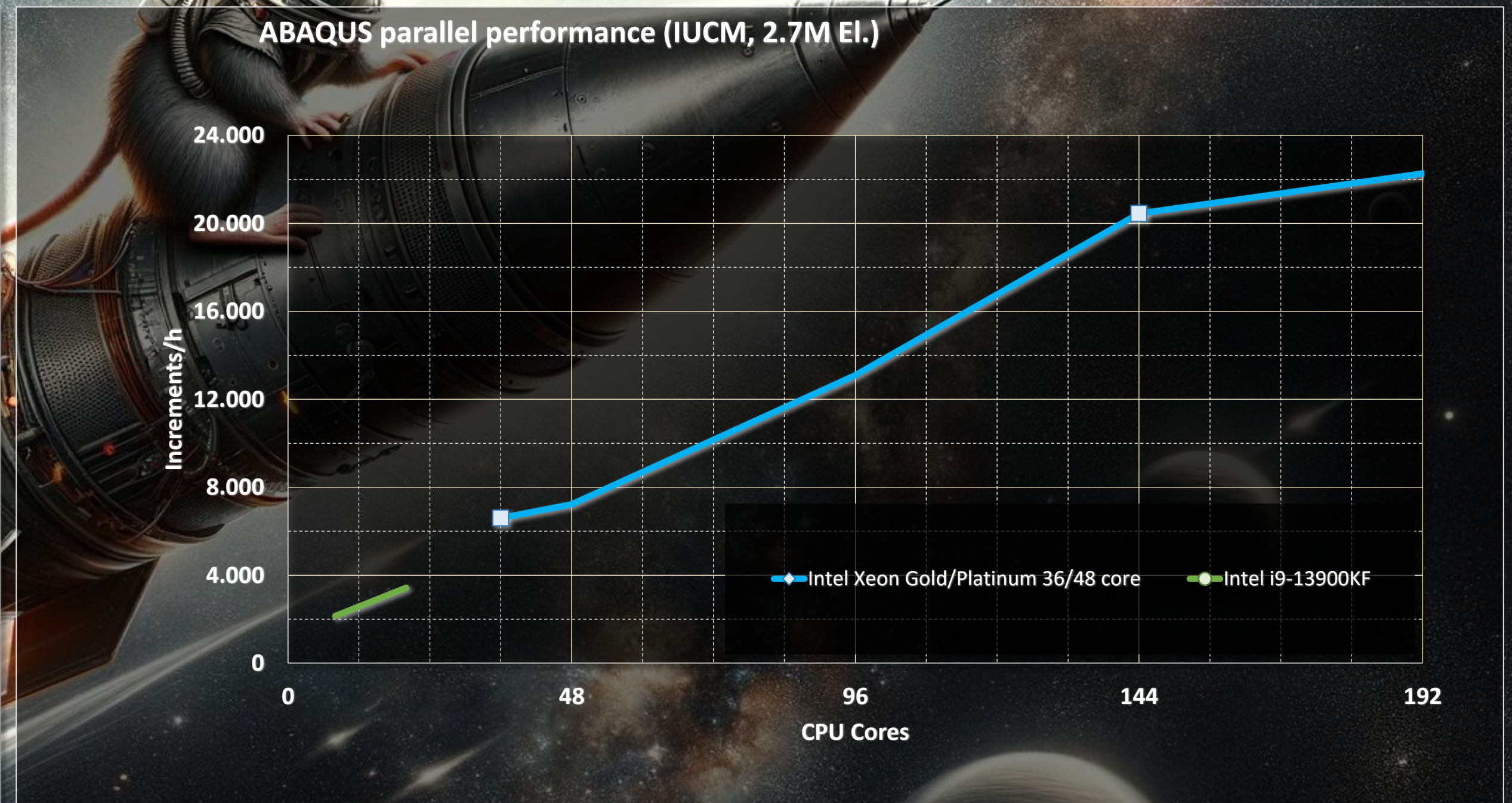
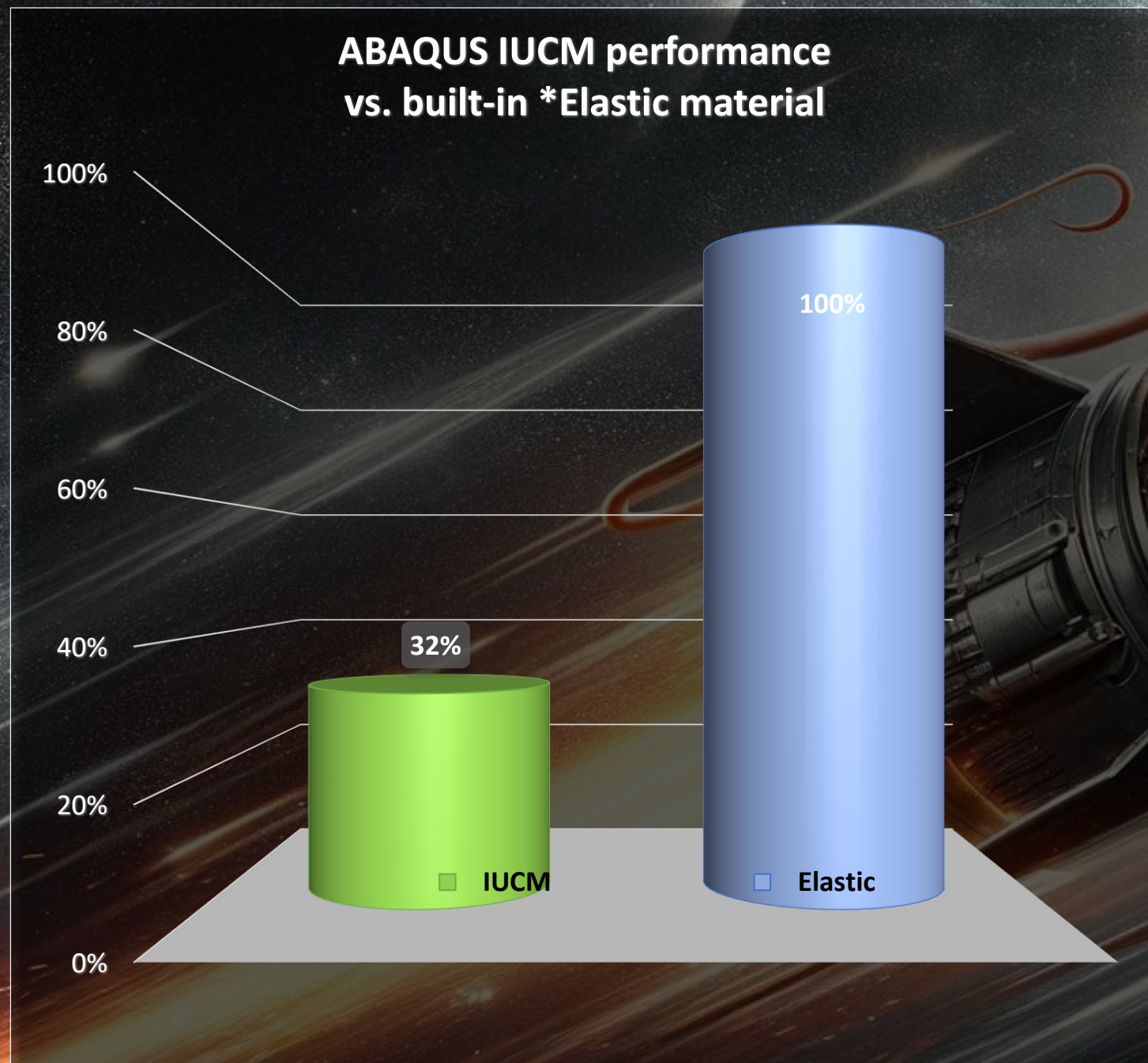
Create simulation



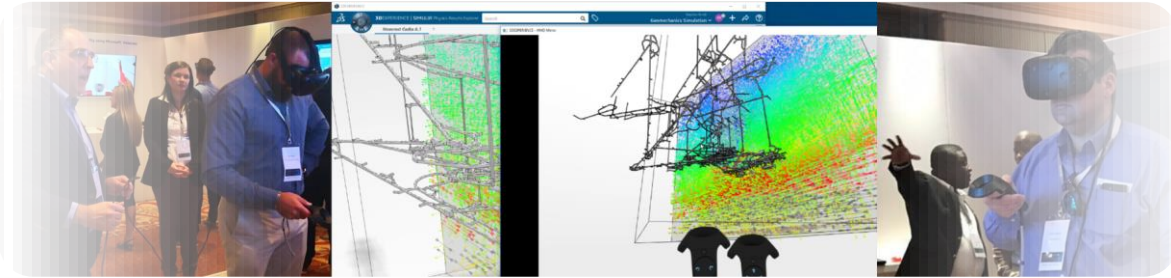
- Research Model A
 - Model
 - Scenario
 - Result
 - BCfield_M2
 - Field Plots (3)
 - Stopes and Development
 - Faults
 - SP3 (Minor Principal)
 - Display Groups (3)



Travelling at the speed of light

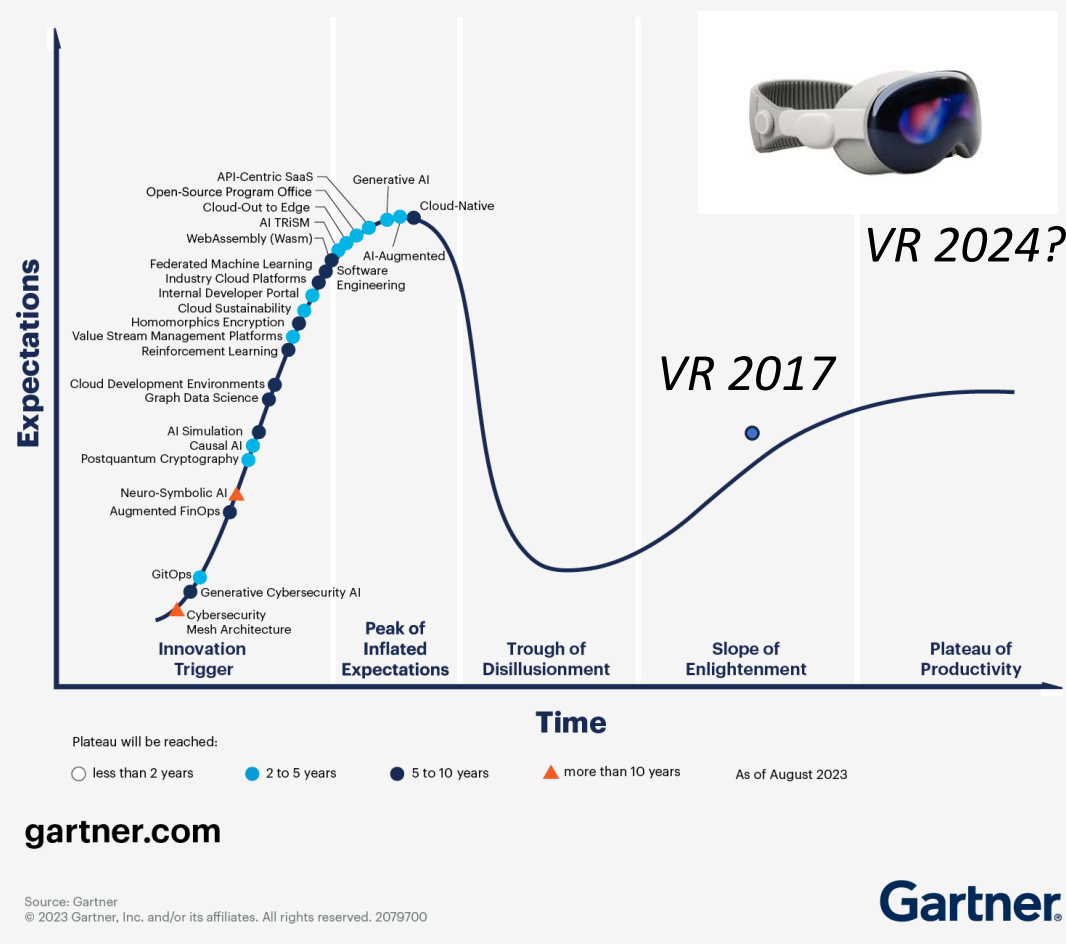


Virtual Reality



Technology Firm Gartner famously booted Virtual Reality (VR) off its “Emerging Technologies” Hype Cycle graph in 2018

Hype Cycle for Emerging Technologies, 2023



Noteworthy: the dominance of AI in 2023

3DEXPERIENCE | SIMULIA Physics Results Explorer

Stephan Arndt

Geomechanics Simulation

Newcrest Cadia A.1

Plots

3DEXPERIENCE: Underground geometry 'as-built' and simulation for Newcrest's Cadia Mine

<https://youtu.be/u7cfXFDGnac?si=hDpdORjCSLPHBU5q>

<https://www.linkedin.com/pulse/virtual-reality-where-business-value-stephan-arndt/>

Thank You

THANK YOU FOR YOUR INTEREST

